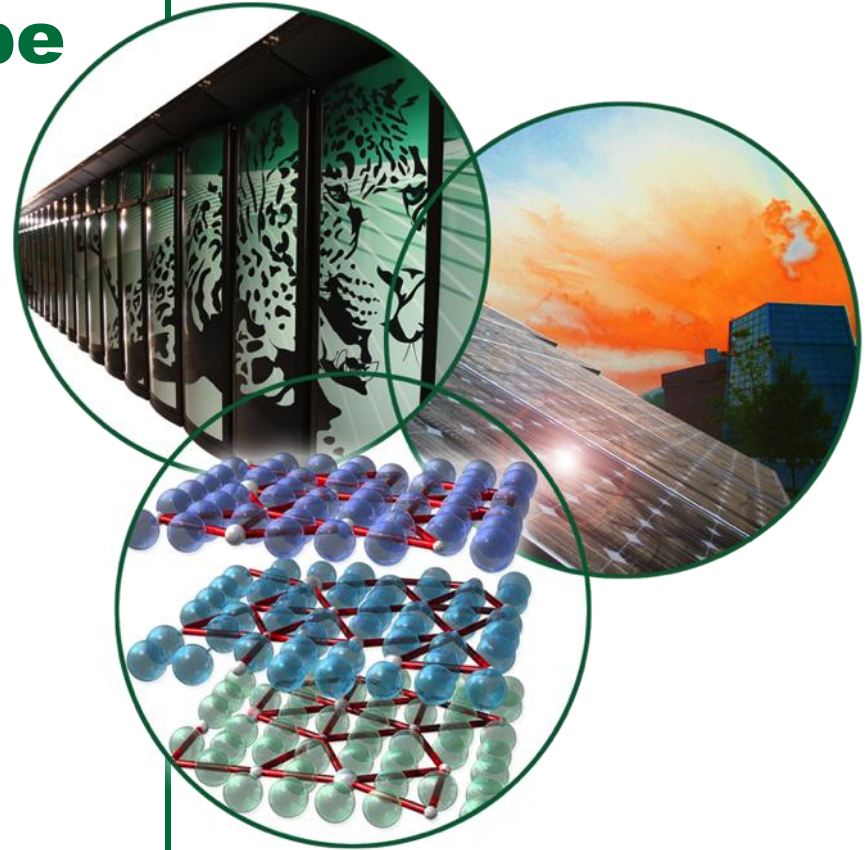


# COMSOL Simulations for Steady State Thermal Hydraulics Analyses of ORNL's High Flux Isotope Reactor (HFIR)

COMSOL  
CONFERENCE  
BOSTON  
2012

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October 03, 2012



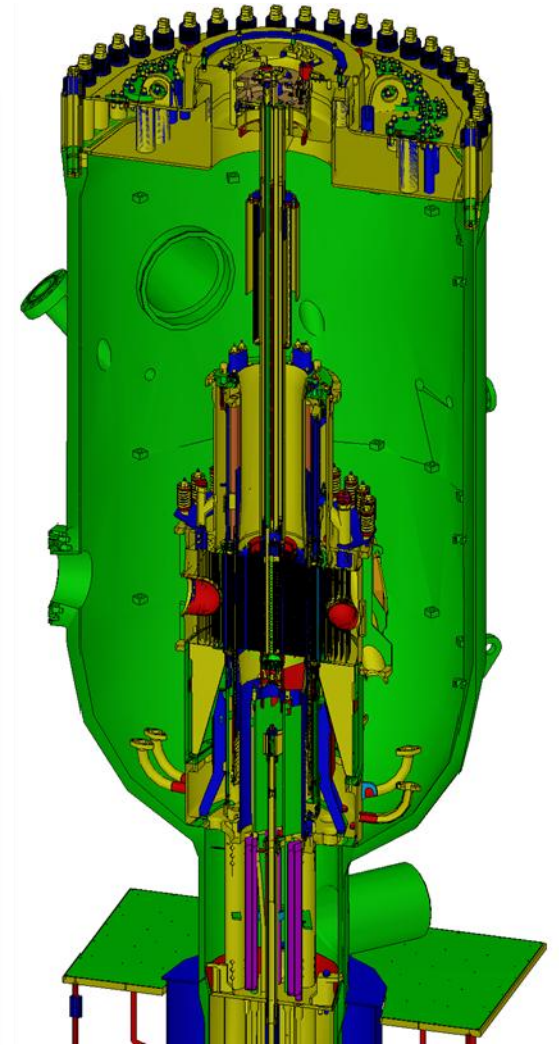
Excerpt from the Proceedings of the 2012 COMSOL Conference in Boston



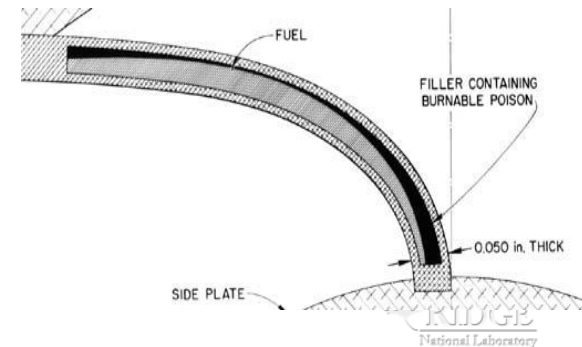
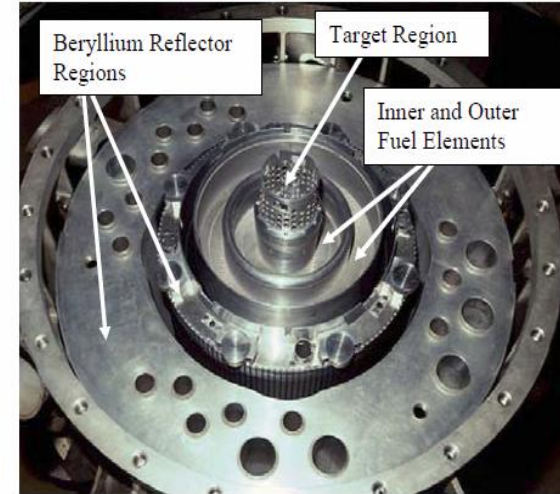
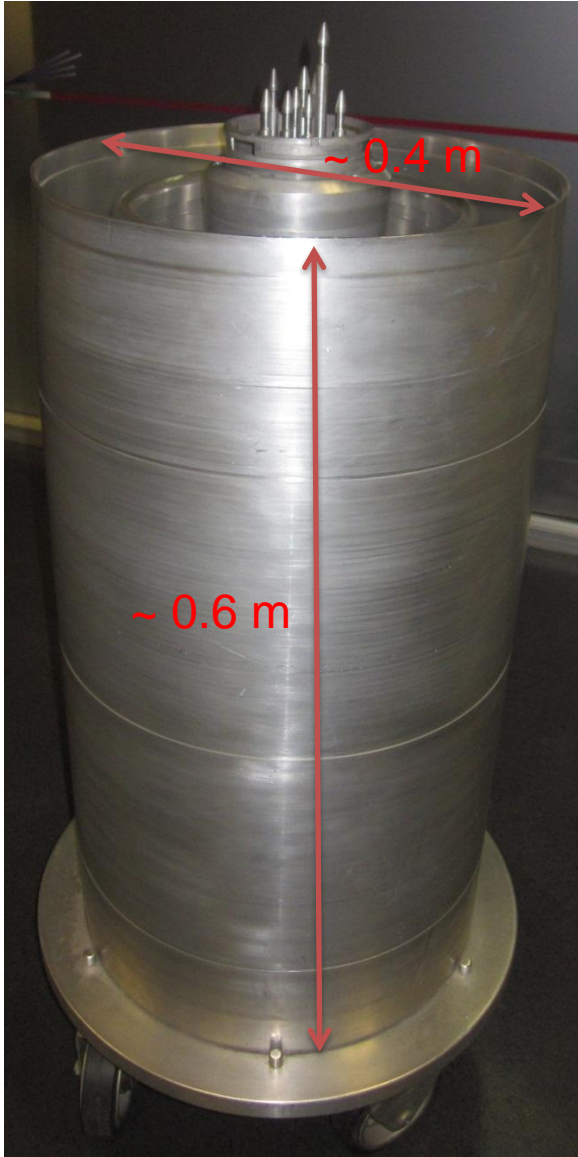
# HFIR is a Multi-Purpose High-Performance Research Reactor



- Operated since 1966 with one of the world's highest thermal neutron fluxes  $\sim 2.5 \times 10^{15}$  neutrons/(cm<sup>2</sup>-s)
- Involute-shaped fuel plates, beryllium reflected, light water-cooled and -moderated, pressurized, flux-trap type research reactor
- Highly enriched uranium ( $\sim 93\%$  <sup>235</sup>U/U) fuel embedded in aluminum-6061 clad
- Cold and thermal neutron scattering, materials irradiation, isotope production, neutron activation analysis



# The HFIR Core



# Physics of Interest for HFIR LEU Safety Analyses

Reactor  
Physics

Turbulent  
Flows

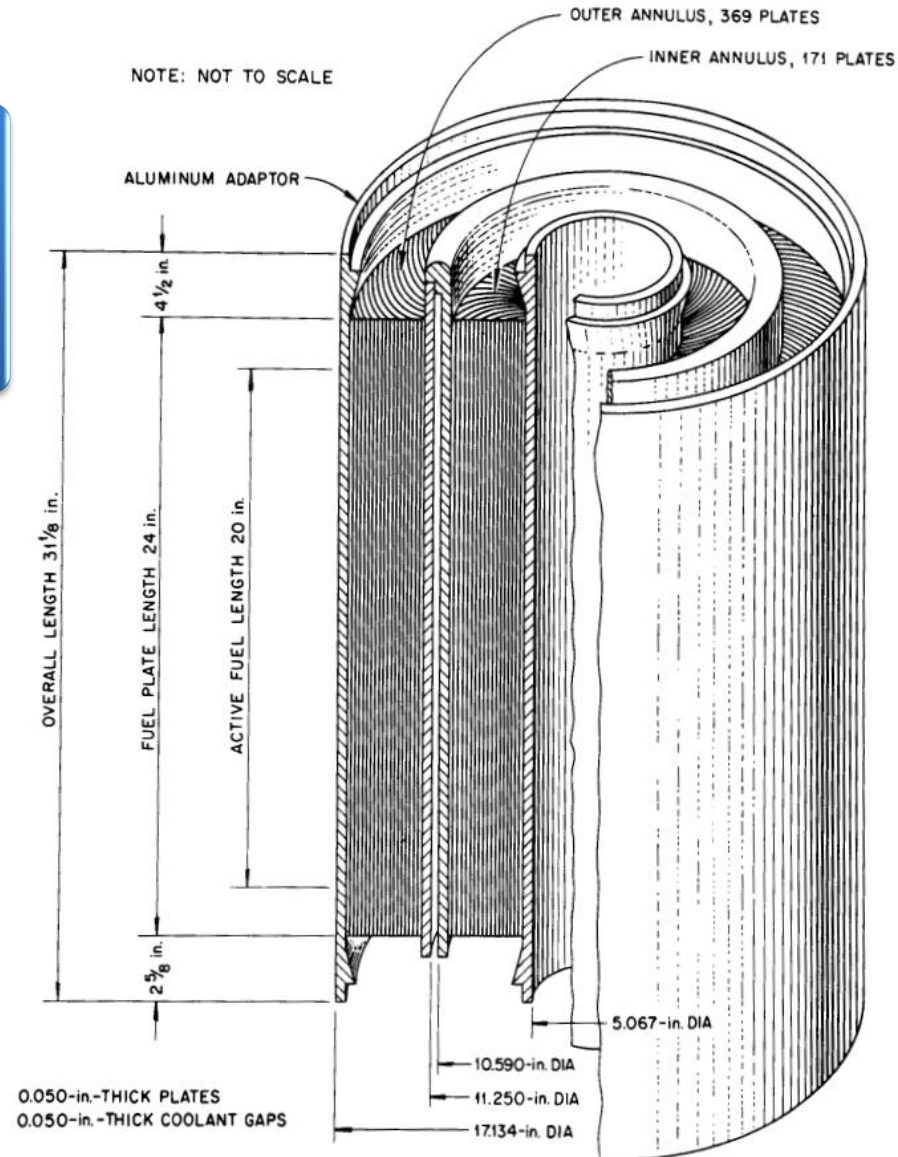
Conjugate  
Heat  
Transfer

Thermal  
Structural  
Interaction  
(TSI)

Fluid  
Structural  
Interaction  
(FSI)

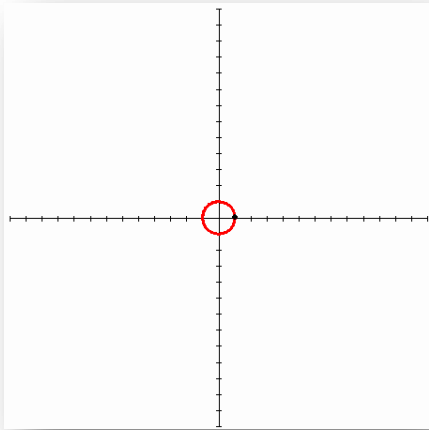
## • Unique features for HFIR modeling

- Multi-physics problem
- Non-uniform spatial heat source distribution inside the fuel plates (fuel, mixture, clad, radial and axial variation)
- Nonlinear material property variation ( $\sim f(T)$ )
- Very narrow flow channels
  - High aspect ratio =  $H/t = 24 \text{ inch} / 0.05 \text{ inch} = 480$
- Desired high level of accuracy and fidelity because of impacts on nuclear safety

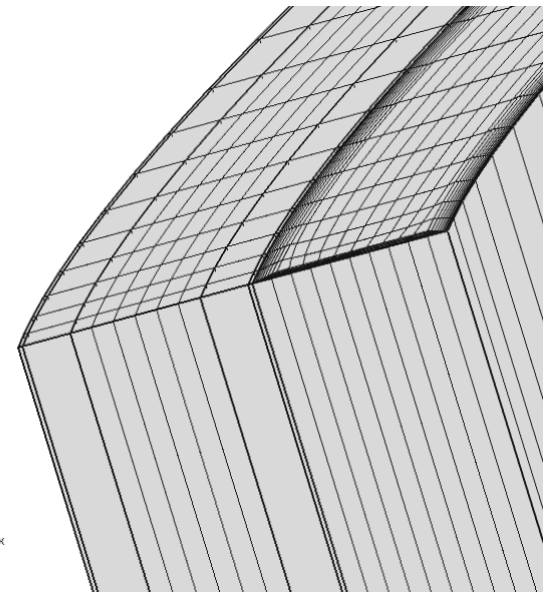
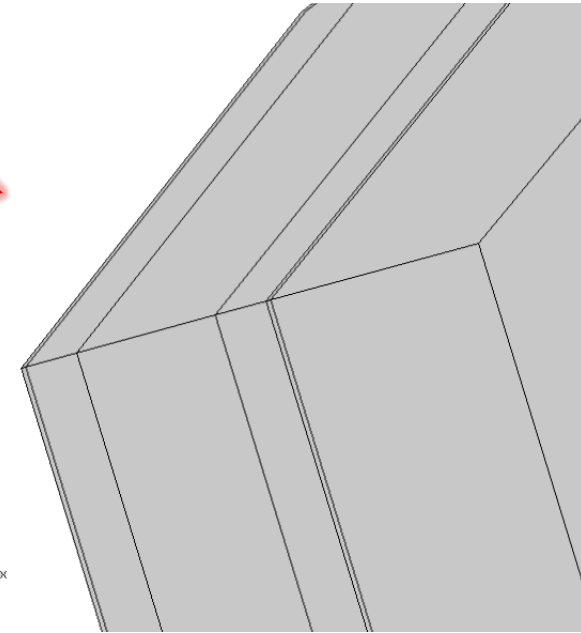
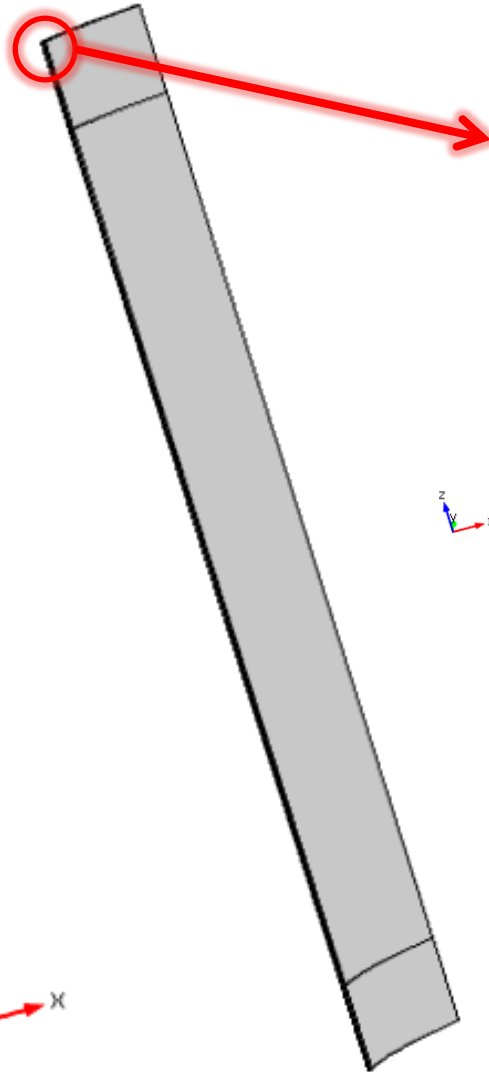


# Parametric Geometry and Mapped Meshing

$$\begin{aligned}x(s) &= R_{b_i} [\sin(s) - s \cdot \cos(s)], \\y(s) &= R_{b_i} [\cos(s) + s \cdot \sin(s)], \quad \text{where} \\ \theta_{\min} &\leq s \leq \theta_{\max}, \\ R_{b_i} &= \text{base radius of the involute, and} \\ \theta_{\min} &= \text{angle for the starting point of the involute, and} \\ \theta_{\max} &= \text{angle for the end point of the involute.}\end{aligned}$$



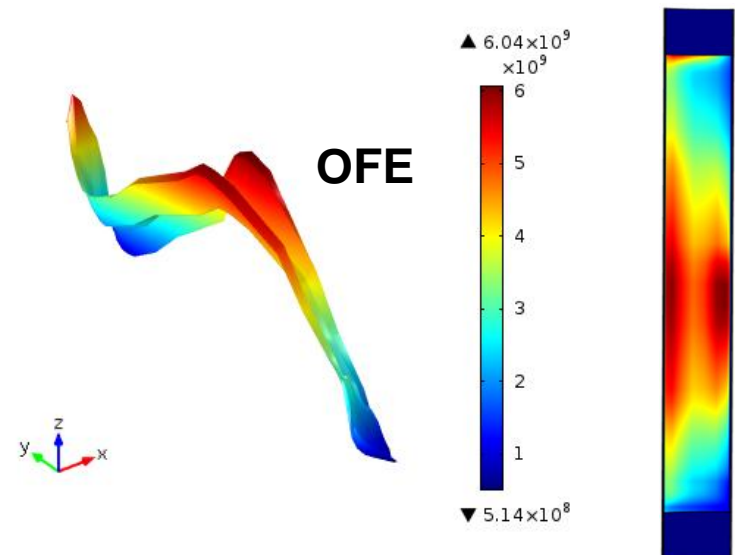
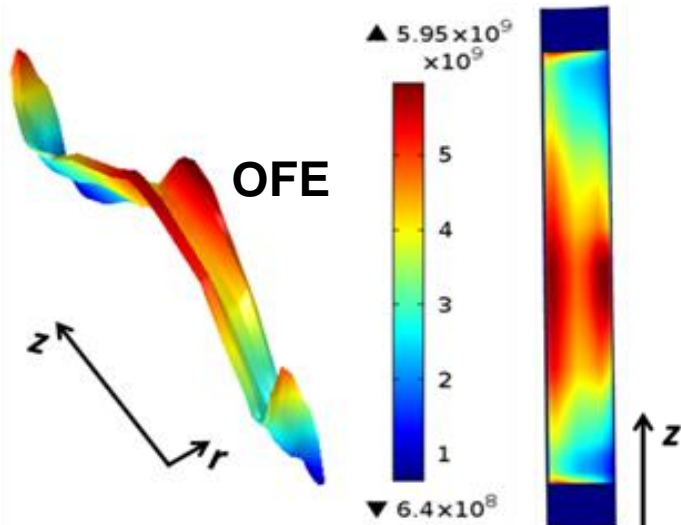
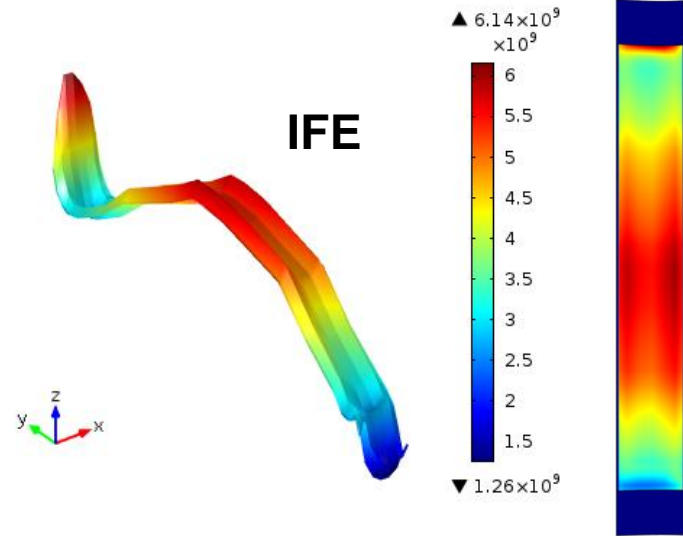
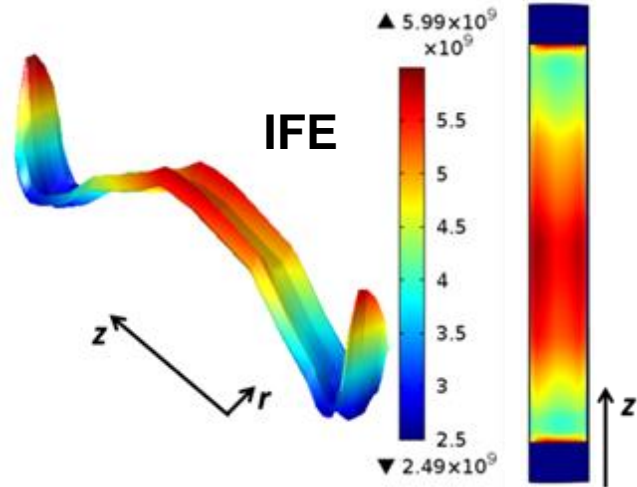
Equation of the involute  
of a circle



# Volumetric Heat Source Distributions

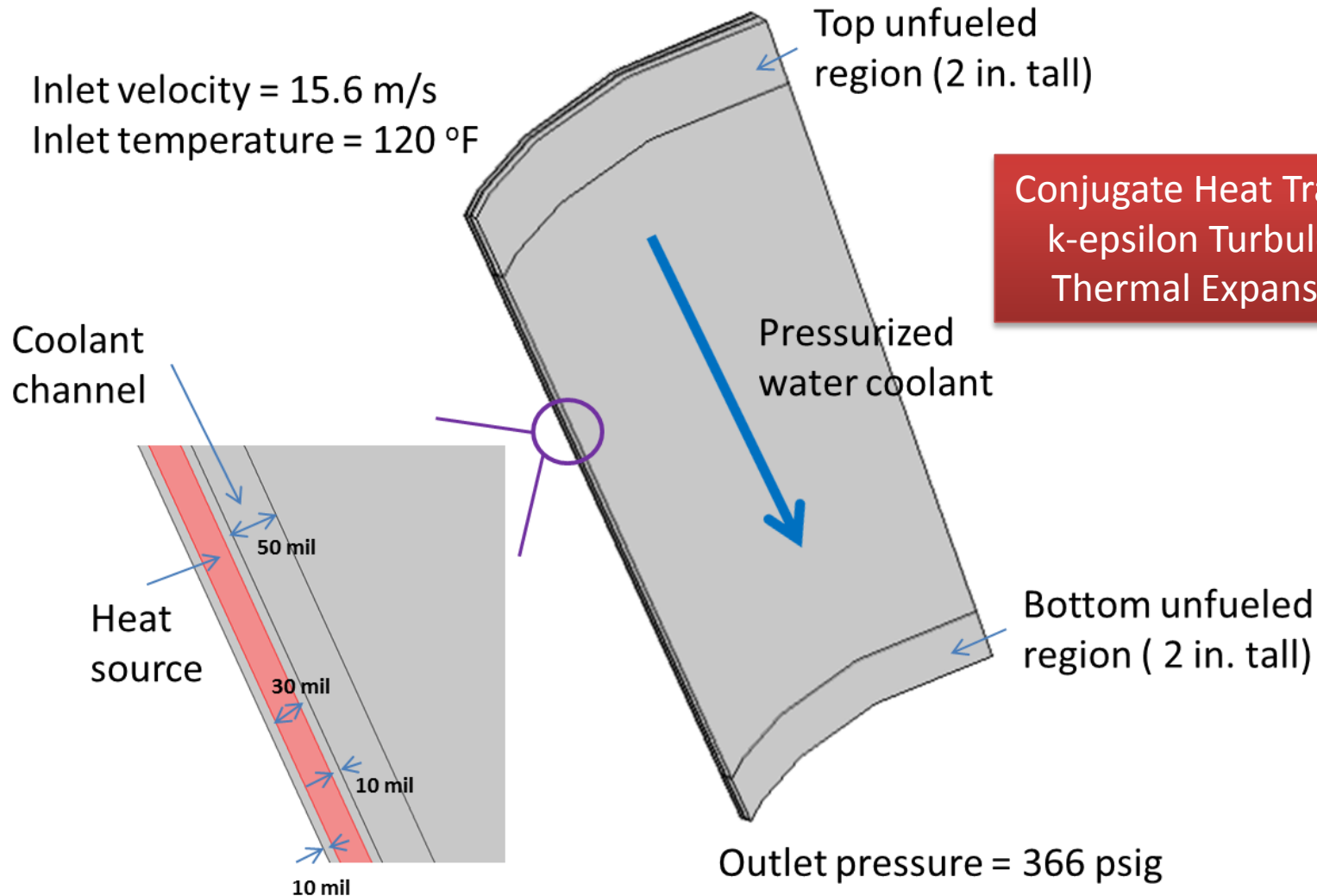
## Axially Non-Contoured Fuel Plates

## Axially Contoured Fuel Plates



# Simulation for Nominal Operation at the Beginning of Reactor Cycle

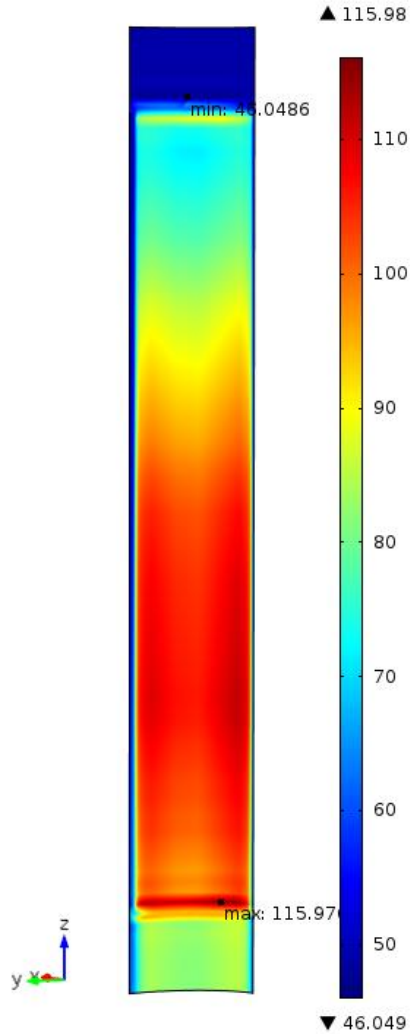
Inlet velocity = 15.6 m/s  
Inlet temperature = 120 °F



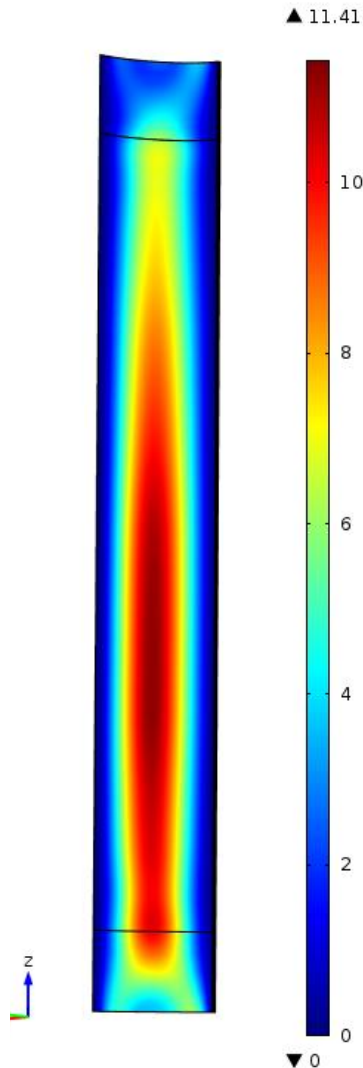
Conjugate Heat Transfer Physics  
k-epsilon Turbulence Model  
Thermal Expansion Physics

# Inner Fuel Element – Nominal Conditions

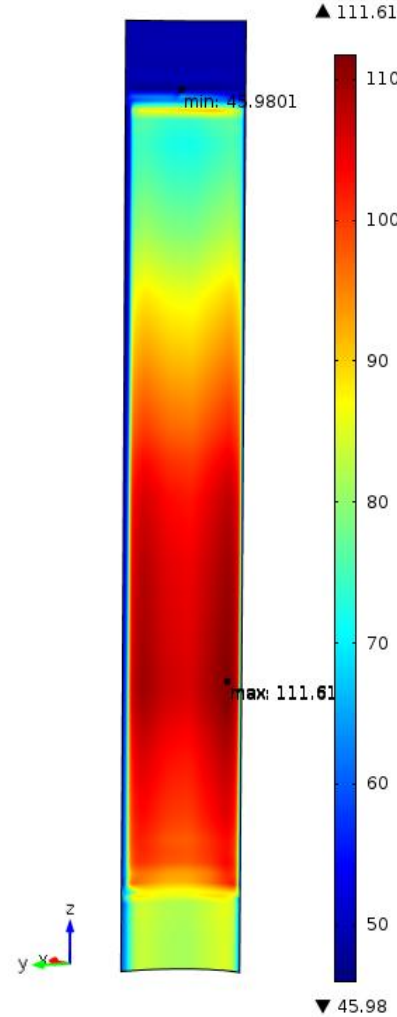
Surface: Temperature (degC)  
Max/Min Surface: Temperature (degC)



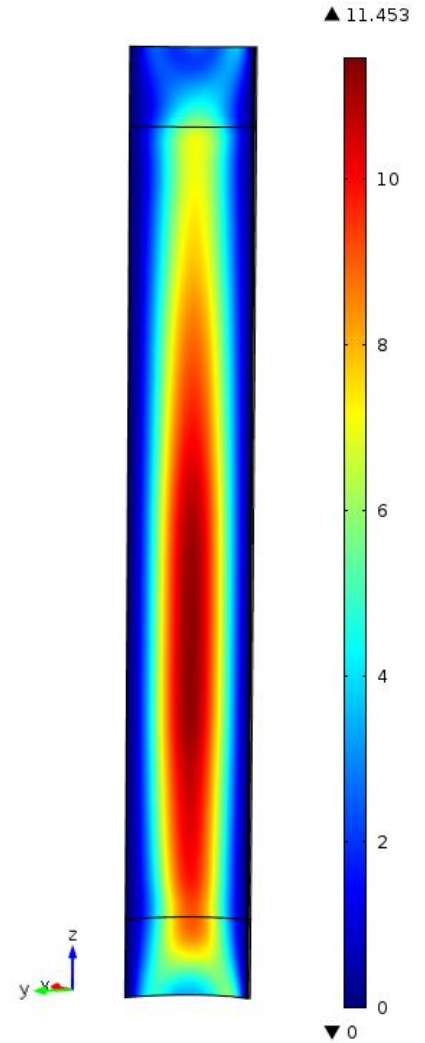
Surface: Total displacement (mil)



Surface: Temperature (degC)  
Max/Min Surface: Temperature (degC)



Surface: Total displacement (mil)



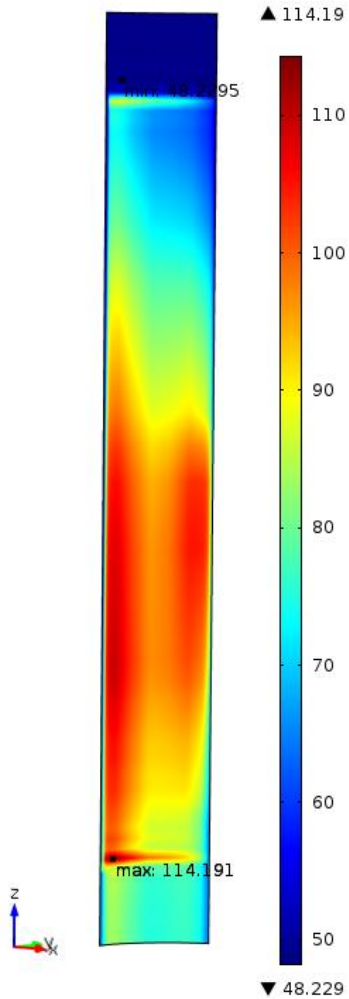
**Axially Non-Contoured Fuel Plates**

**Axially Contoured Fuel Plates**

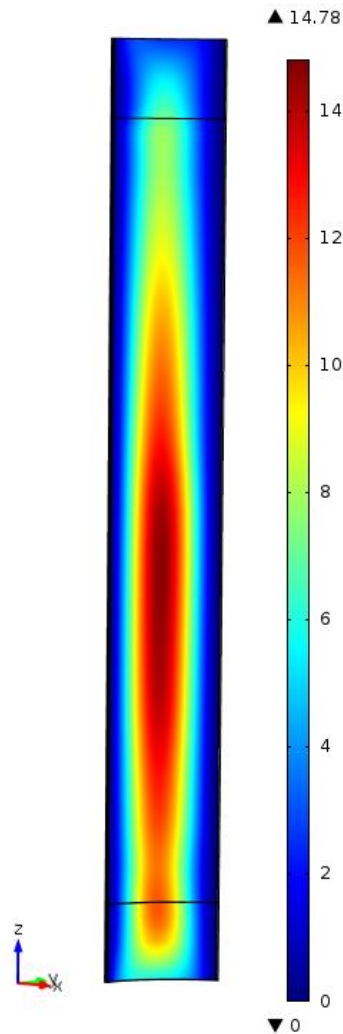


# Outer Fuel Element – Nominal Conditions

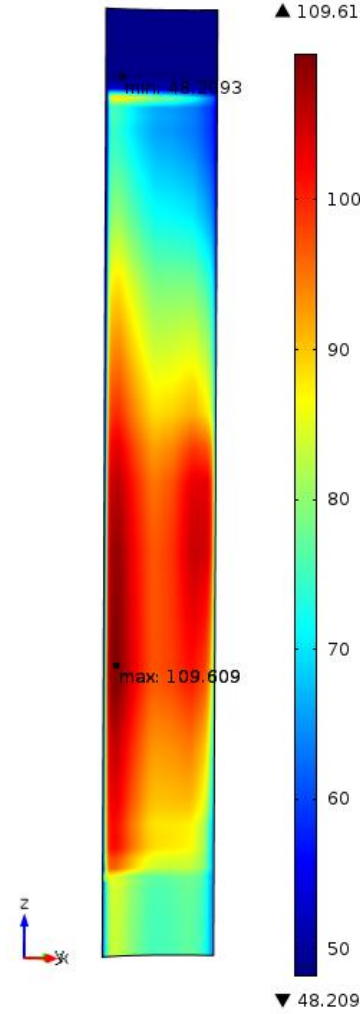
Surface: Temperature (degC)  
Max/Min Surface: Temperature (degC)



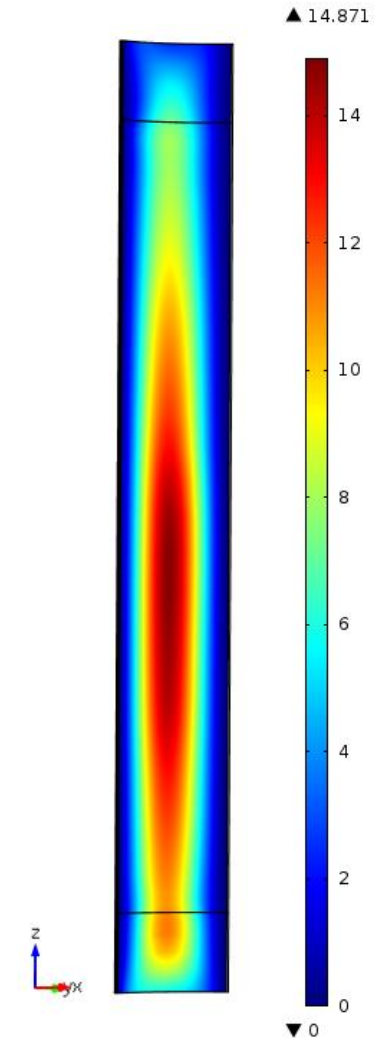
Surface: Total displacement (mil)



Surface: Temperature (degC)  
Max/Min Surface: Temperature (degC)



Surface: Total displacement (mil)



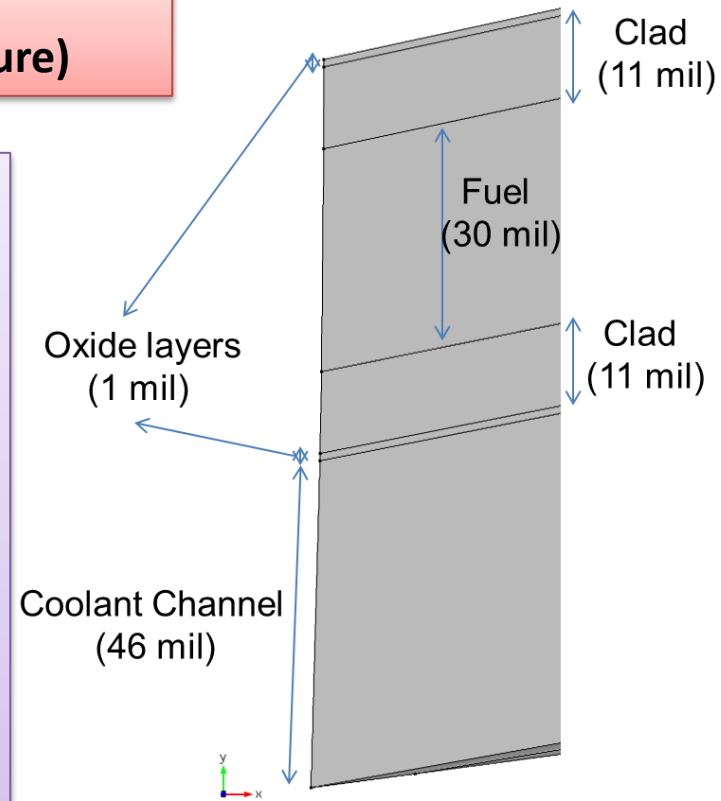
**Axially Non-Contoured Fuel Plates**

**Axially Contoured Fuel Plates**

# “Hot Channel” Safety Basis Cases at the Beginning Of Cycle

Conservative boundary conditions  
(135 °F inlet temperature and 232.7 psia outlet pressure)

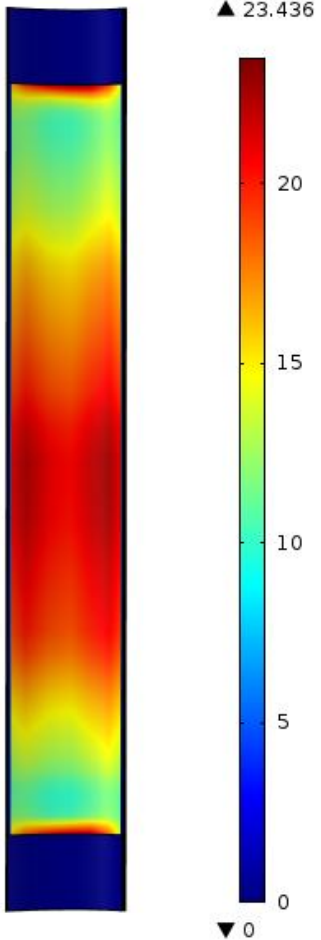
- U2 = Uncertainty in the fissile loading = **1.05**
- U3 = Uncertainty in the power density distribution = **1.199**
- U4 = Uncertainty in average fuel concentration in hot plate = **1.06**
- U18 = Fuel Segregation Flux Peaking = **1.1**
- $U_{eff} = U2 * U3 * U4 * U18 = \mathbf{1.4679}$
- Effective heat source =  
 **$U_{eff} * PowerFactor * MCNP\_Power$**



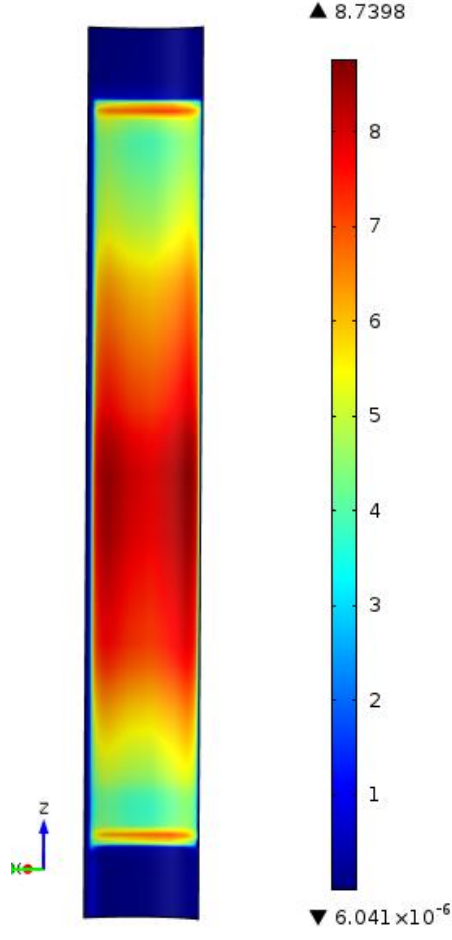
# IFE, Axially Non-Contoured LEU Fuel

Power Factor = 1.6

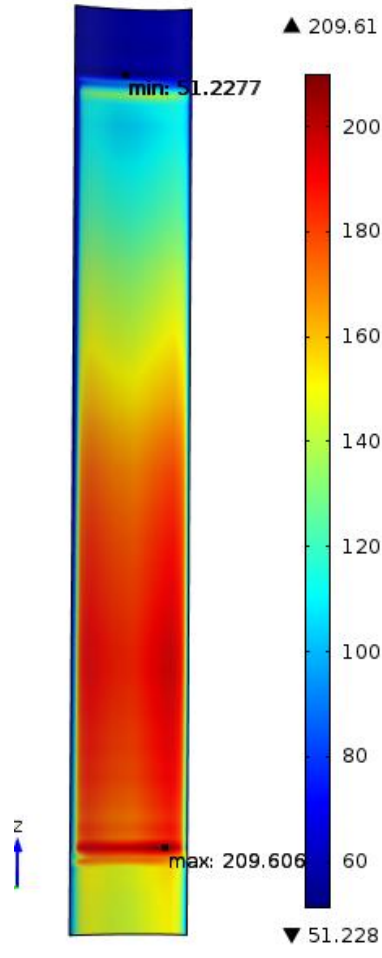
Power\_Factor(4)=1.6  
Volume: Total heat source (GW/m<sup>3</sup>)



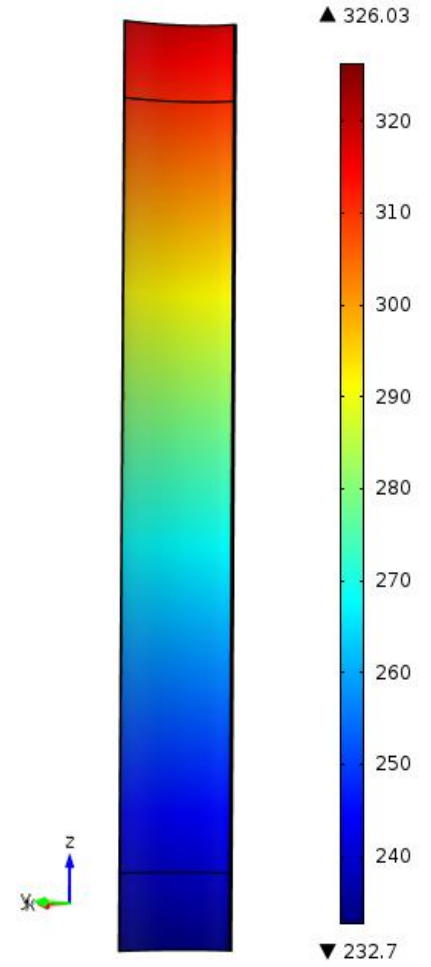
Power\_Factor(4)=1.6  
Surface: Total heat flux magnitude (MW/m<sup>2</sup>)



Surface: Temperature (degC)  
Max/Min Surface: Temperature (degC)



Power\_Factor(4)=1.6 Surface: Pressure (psi)



Heat Source  
( $Q'''$ )

of Energy

Clad Heat Flux  
( $q''$ )

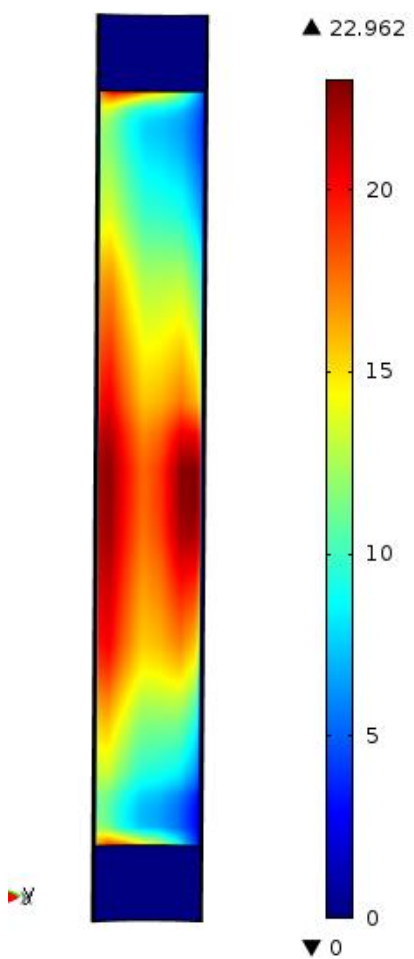
Clad Temperature  
( $T$ )

Coolant Pressure  
( $P$ )

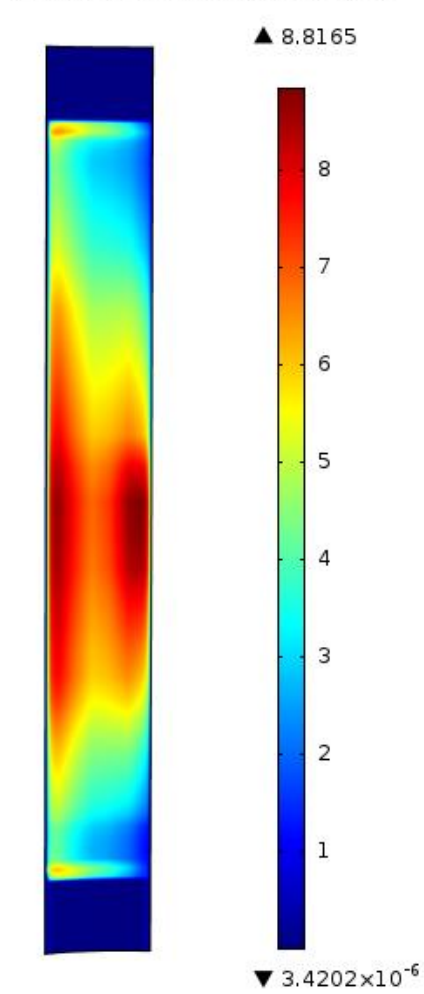
# OFE, Axially Non-Contoured LEU Fuel

Power Factor = 1.6

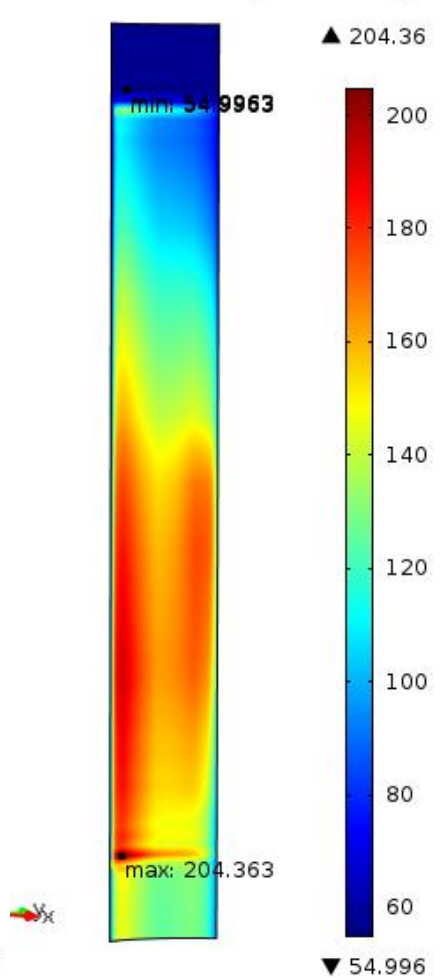
Power\_Factor(4)=1.6  
Volume: Total heat source (GW/m<sup>3</sup>)



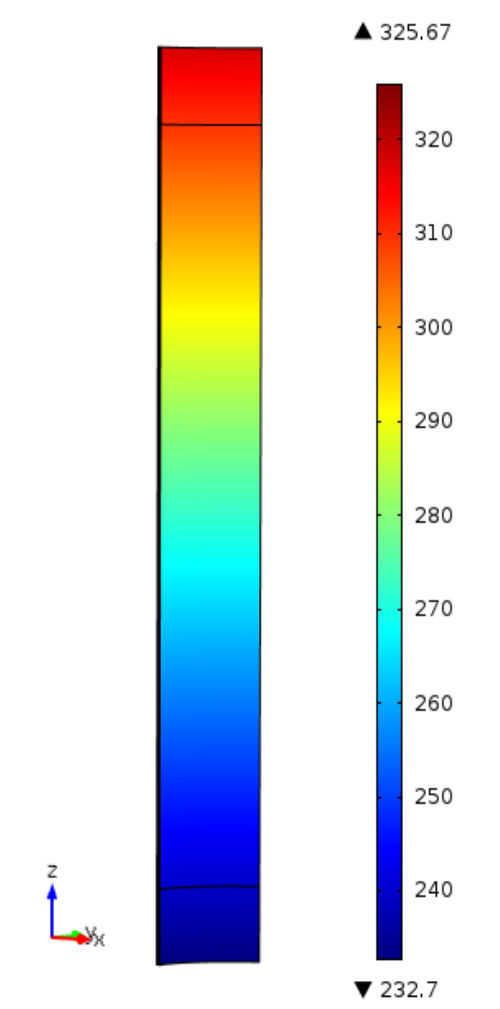
Total heat flux magnitude (MW/m<sup>2</sup>)



Surface: Temperature (degC)  
Max/Min Surface: Temperature (degC)



Power\_Factor(4)=1.6 Surface: Pressure (psi)



Heat Source  
(Q''')

Clad Heat Flux  
(q'')

Clad Temperature  
(T)

Coolant Pressure  
(P)

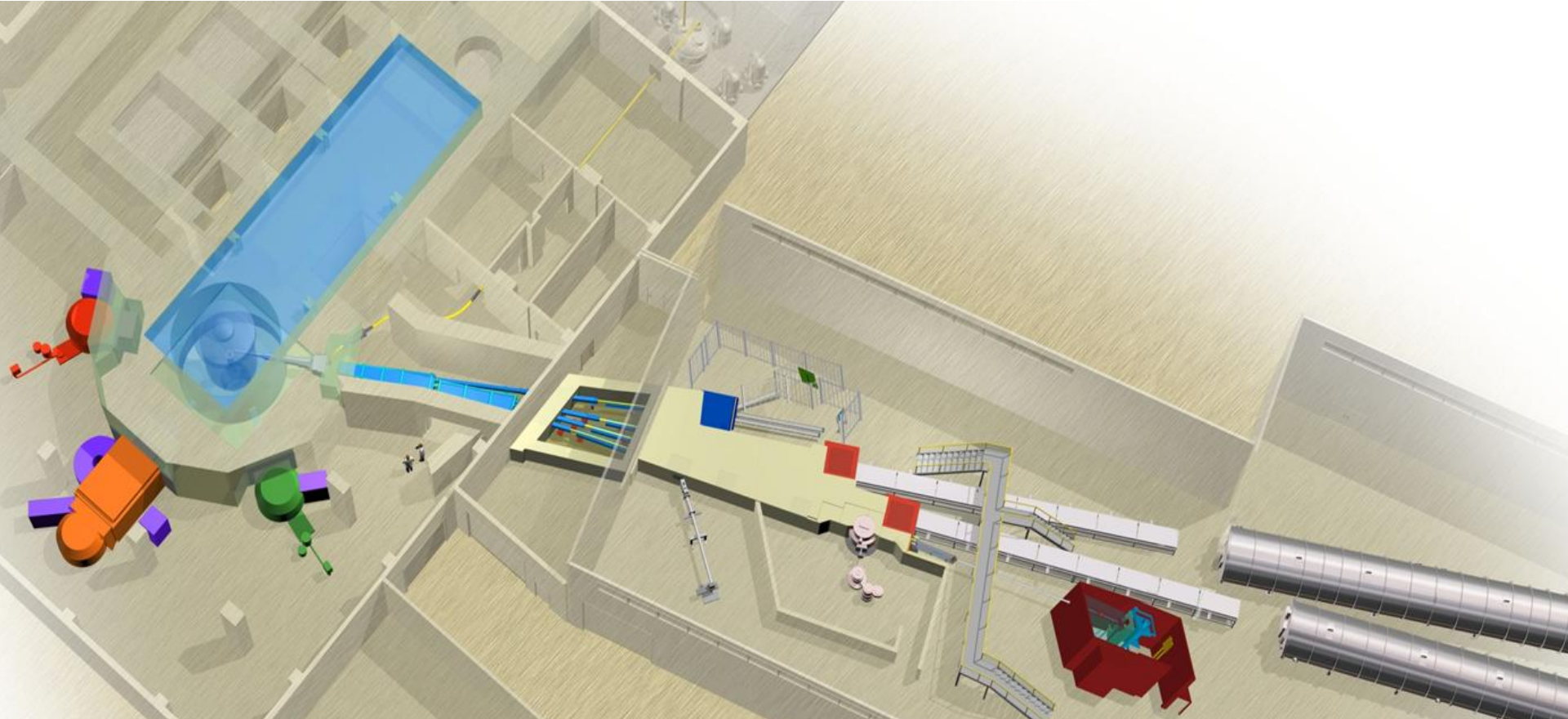
of Energy

psi

# Conclusions and Future Directions

- COMSOL Multiphysics is providing a robust platform to simulate HFIR fuel plates and coolant channels.
- Models developed for IFE and OFE are continually being advanced with a goal to simulate HFIR's safety basis conditions (or, worst possible conditions).
- Preliminary work is also underway to develop a one-dimensional HFIR system model with the primary/secondary piping loops, heat exchangers, pumps, valves and bends. This model is based on HFIR's existing RELAP5 models.
- Coupled CFD/SM models of IFE and OFE could later be coupled with the HFIR system model.
- Parallel and scalable solvers in COMSOL need to be improved and made easier to implement to allow significantly "bigger" HFIR simulations on leadership class computing clusters (e.g., Jaguar/Titan, Kraken etc.).

# Thank you for your attention.



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