

STUDY OF ELECTROCHEMICALLY GENERATED TWO-PHASE FLOWS

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Savoie)

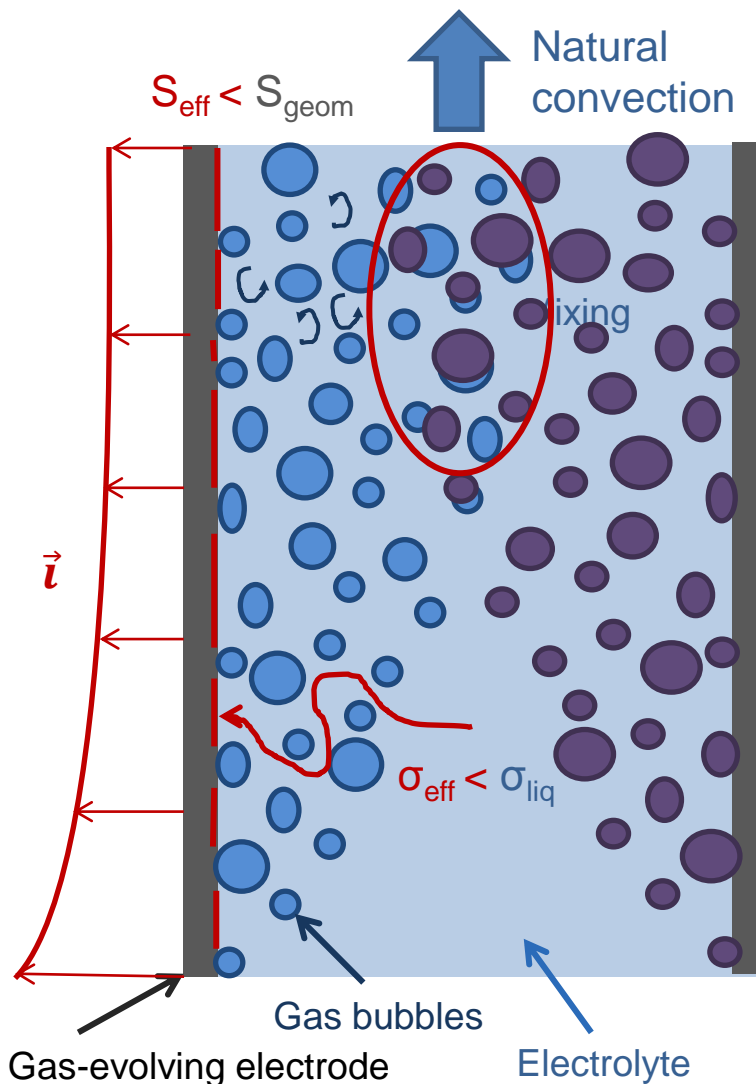
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1 - CONTEXT

1.1 – CONTEXT : GAS GENERATION DURING ELECTROCHEMICAL PROCESSES

- **Gas bubbles** are frequently generated in electrochemical processes
 - **As principal product** (e.g. in electrolysis)
 - High **gas recuperation rate** must be reached
 - **As a by-product** (e.g. in electrodeposition)
 - **Negative impact** on the principal reaction should be avoided
- Bubbles behavior in electrolyte **strongly affects process performances**

1.1 – CONTEXT : GAS GENERATION DURING ELECTROCHEMICAL PROCESSES



o Bubble-induced

- **Natural convection**

- **Mixing**

- **Surface coverage**

- **Mass transfer limitation**

- **Bulk conductivity drop**

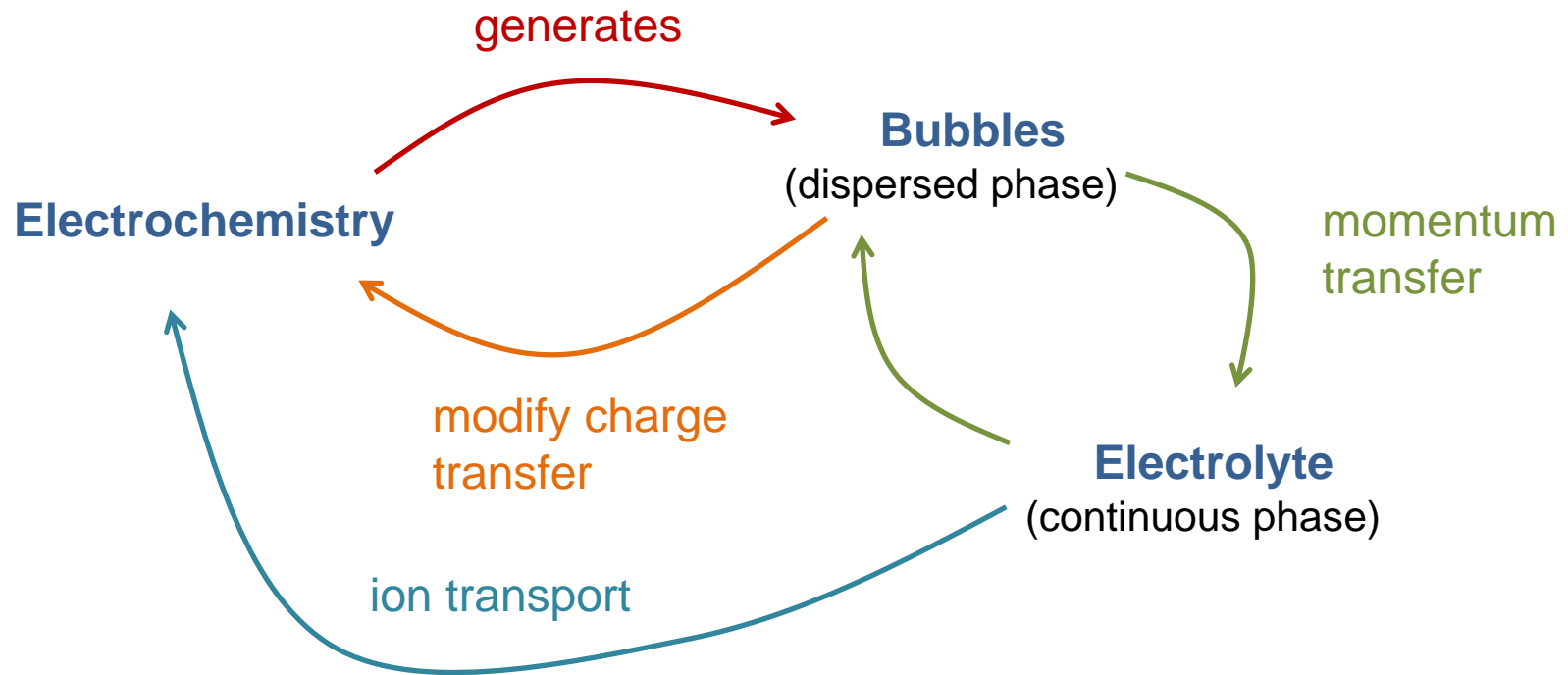
- **Current limitation**

o Risk of plume mixing

- **Decreased yield**

- **Energy production ($\text{H}_2 + \text{O}_2$)**

1.2 - PHYSICAL INSIGHT TO ENHANCE CELL'S DESIGN



Strong coupling between physical phenomena

- Difficulty to **control the process**
- Numerous parameters for **empirical analysis**
- Necessity of a **realistic model**

2 – MODEL DESCRIPTION, RESULTS AND DISCUSSION

2.1 - MIXTURE MODEL^[1]

- CFD equations : Laminar, Newtonian fluid, $\rho_D \ll \rho_C$, **void fraction α**

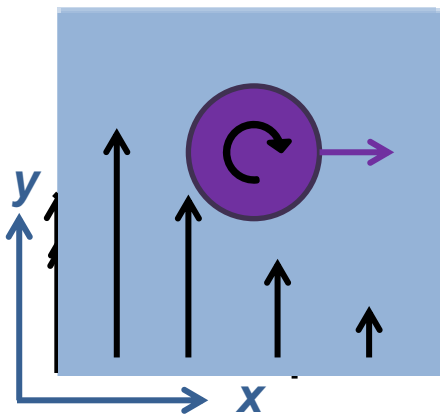
$$\vec{\nabla} \cdot \vec{U} = 0 \quad (\text{Mixture volume conservation})$$

$$\vec{\nabla} \cdot \vec{U}_D = 0 \quad (\text{Dispersed phase volume conservation})$$

$$\rho_C(1 - \alpha)\vec{q} \cdot \nabla \vec{q} = -\vec{\nabla} P + \rho_C g \alpha \vec{z} + \left(\vec{\nabla} \cdot [\mu(\alpha)(\nabla \vec{q} + \nabla \vec{q}^T)] - \vec{\nabla} \left[\frac{2}{3} \mu(\alpha) \vec{\nabla} \cdot \vec{q} \right] \right) \quad (\text{Momentum conservation})$$

- Closure model for relative flux** : small rigid spheres approximation

$$\vec{U}_R = \vec{U}_D - \alpha \vec{U} = \vec{U}_{Stokes} + \vec{U}_{Hdiff} + \vec{U}_{Sdiff} + \vec{U}_{Smig} + \vec{U}_{Saff} \quad [2]$$



$\vec{U}_{Sdiff} = \frac{0.6\alpha^2}{\tau} \nabla \tau$

Shear induced diffusion in a uniformly sheared plume due to a non-uniform shear concentrated plume

Lift force (Saffman force) of a rotating bubble in a sheared plume

$$\frac{\partial v}{\partial x} \frac{r_b^2 g \rho_C}{\tau} = \frac{f \alpha^2}{3} (1 + 0.5e^{8.8\alpha})$$

hindering junction

[1] M. Ishii, T. Hibiki, Thermo-Fluid Dynamics of Two-Phase Flow, Springer, New York, NY, 2011.

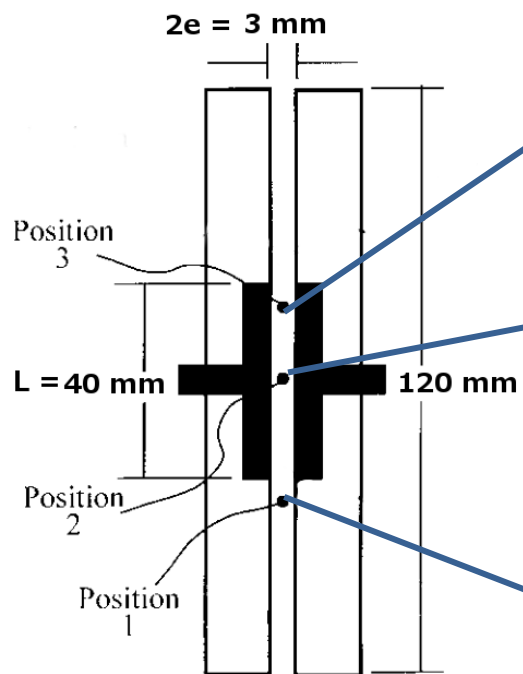
[2] R. Wedin, A.A. Dahlkild, Ind. Eng. Chem. Res. 40 (2001) 5228–5233

2.1 - MIXTURE MODEL : ASSUMPTIONS

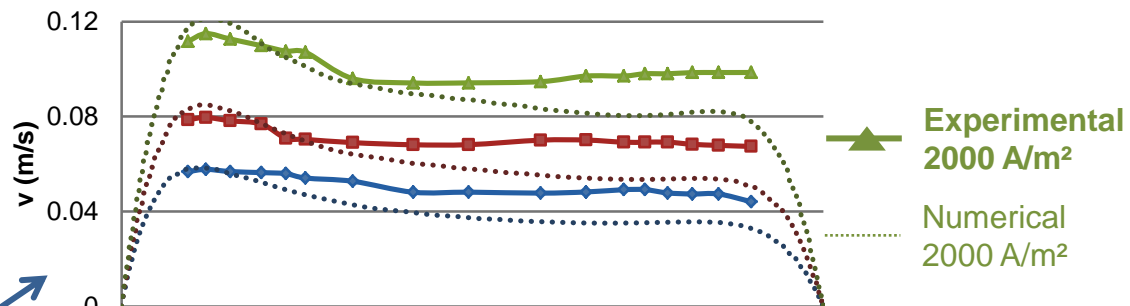
- **Electrokinetics** not computed
 - **Uniform current** approximation
 - **Small influence** on two-phase flow results
- $\nabla C \sim 0$ due to strong **mixing**
- **Heat generation** neglected
 - **Thermal-induced** convection \ll **bubble-induced** convection

2.2 - MODEL VALIDATION : SIMULATING EXPERIMENTAL RESULTS

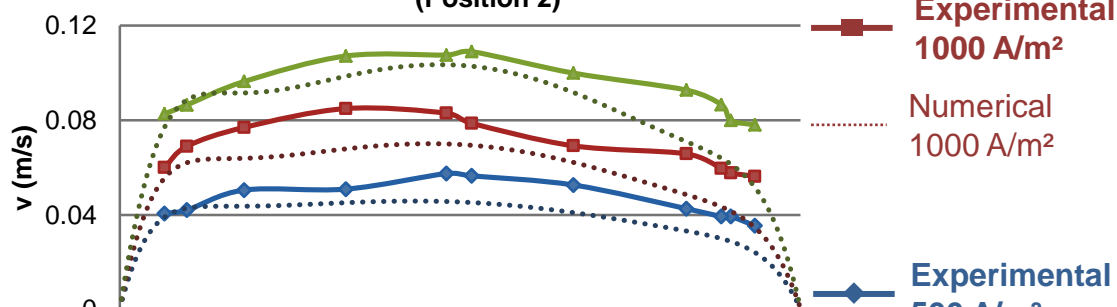
Water alkaline electrolysis, bubble-induced convection



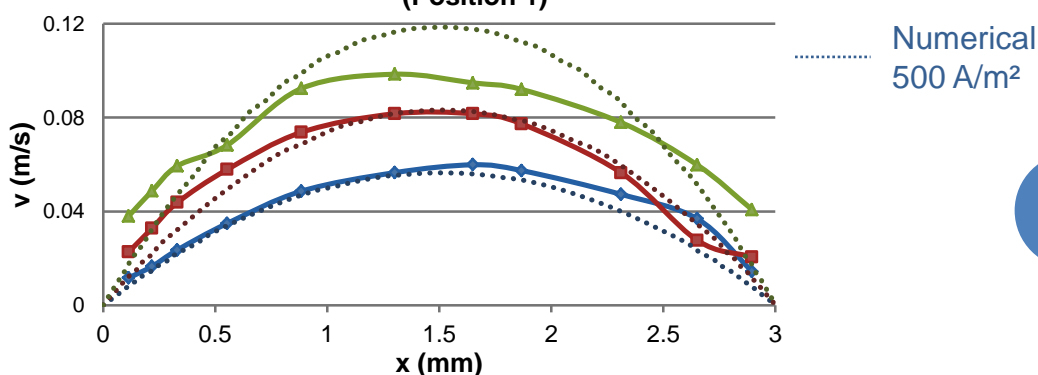
Velocities measured by Byrne & Boissonneau compared to numerical results (Position 3)



(Position 2)



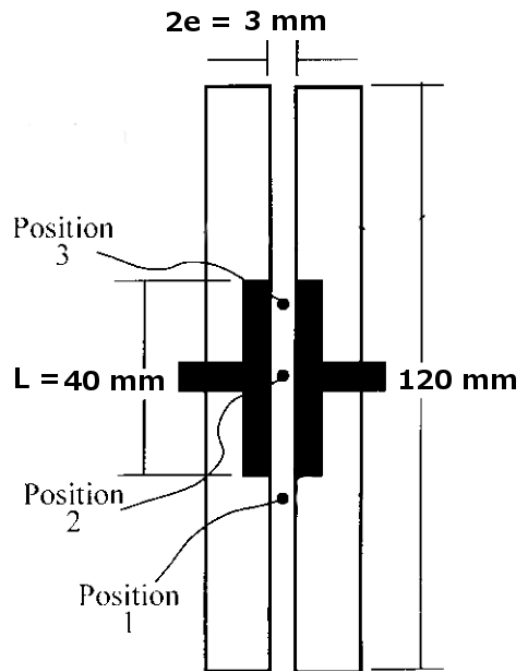
(Position 1)



[3] P. Boissonneau, P. Byrne, J. Appl. Electrochem. 30 (2000) 767–775

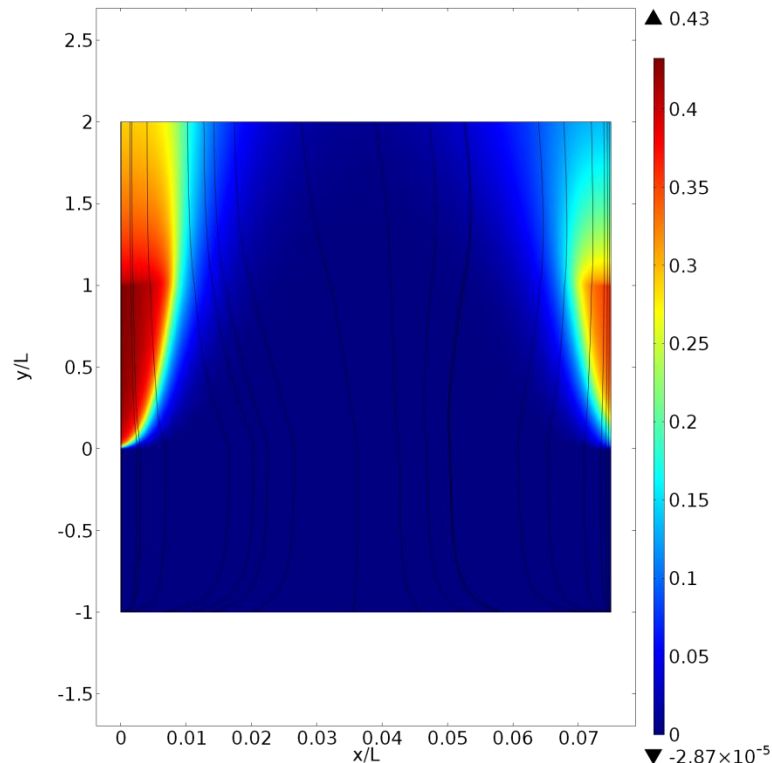
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Void fraction evolution and
streamlines (2000 A/m²)



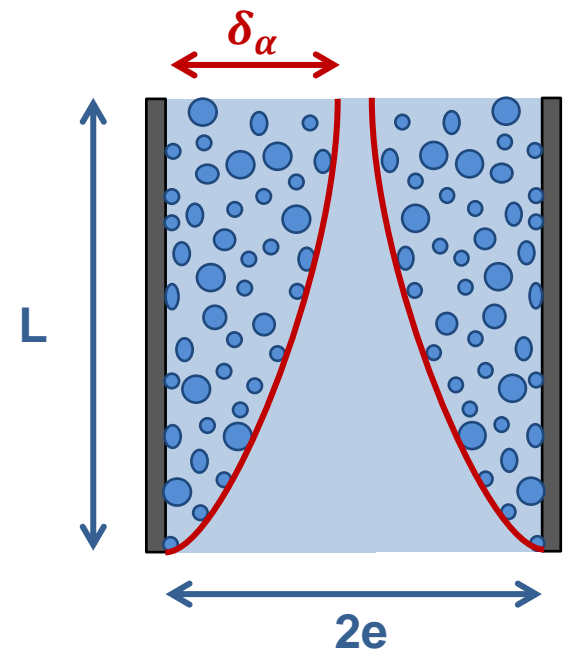
2.3 – CREATING NEW MODEL : THE THERMAL ANALOGY^[4]

- Bubble plume ~ **thermal boundary layer**
 - Buoyancy forces and void fraction concentrated in the vicinity of electrodes
- Dispersed phase conservation ~ **convection-conduction equation**
 - $U_x \frac{\partial \alpha}{\partial x} + U_y \frac{\partial \alpha}{\partial y} = \frac{\partial}{\partial x} \left(K_\alpha \frac{\partial \alpha}{\partial x} \right)$
 - $K_\alpha \sim aU_S$
- Boundary layer thickness **scale analysis**
 - **Rayleigh-like number**

$$Pr_\alpha = \frac{\nu}{K_\alpha}$$

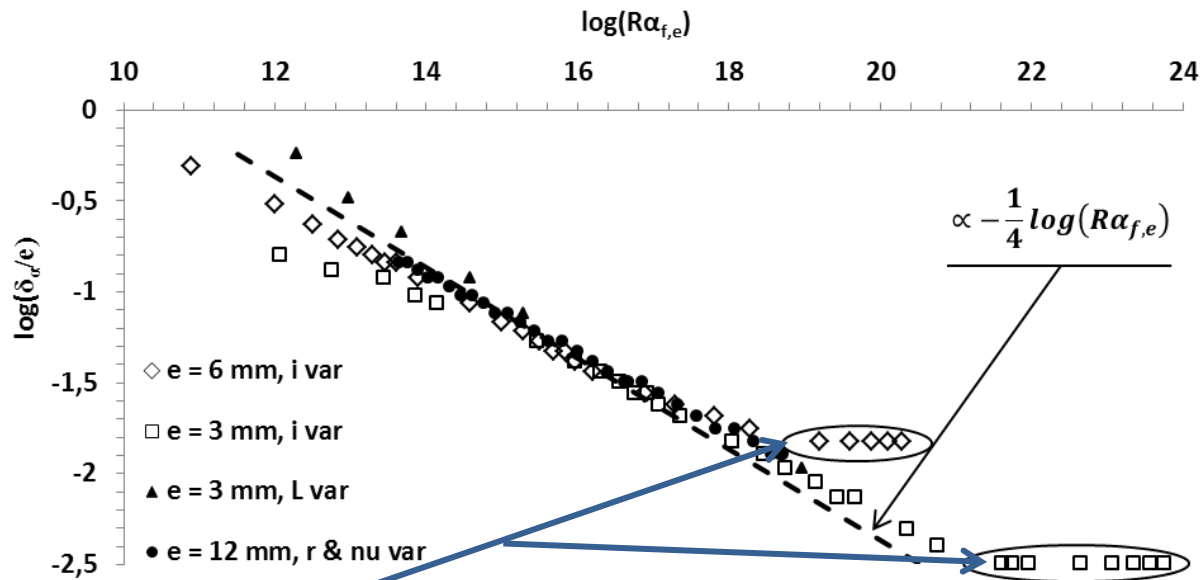
$$Ra_{e,f} = \frac{\nu U_g e^5}{\alpha^6 g L}$$

$$\frac{\delta_\alpha}{e} \sim Ra_{e,f}^{-1/4}$$



2.3 - $PR_\alpha \gg 1$

Relative plume thickness vs. Rayleigh-like number (log-scale)



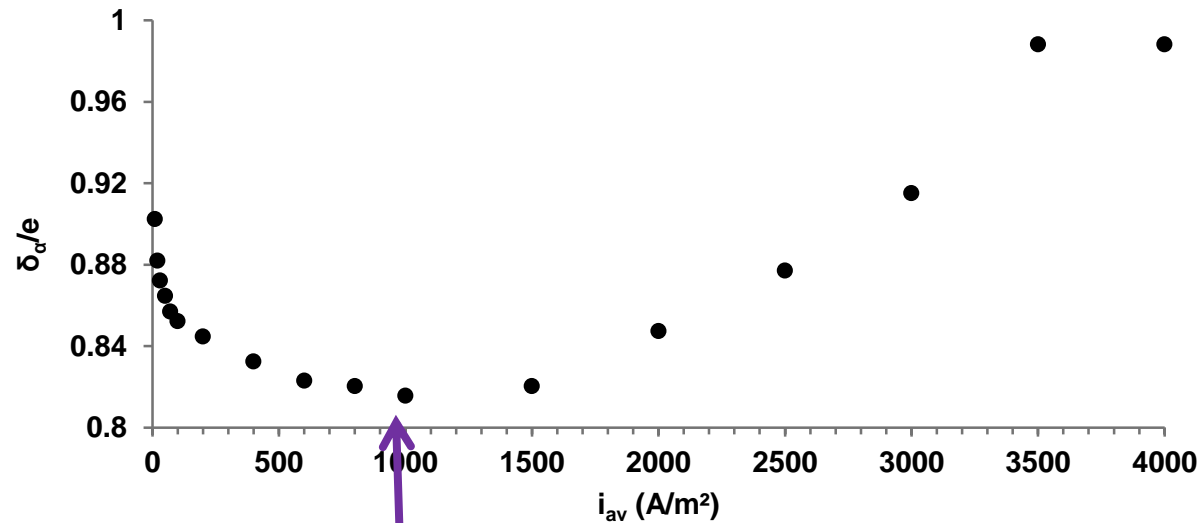
At high currents \rightarrow **Strong shear**
 $\rightarrow U_{Sdiff,x} \ll U_{Hdiff,x} \rightarrow K_\alpha \sim r_b^2 \dot{\gamma}$
 $\rightarrow \frac{\delta_\alpha}{e} \sim \frac{(r_b^2 L)}{e}$

Important result :

$$\frac{\delta_\alpha}{e} \sim \left(\frac{r_b^6 g L}{\nu U_g e^5} \right)^{0,25}$$

2.3 - $PR_\alpha \ll 1$: LIMITING CASE

Relative plume thickness vs. current density



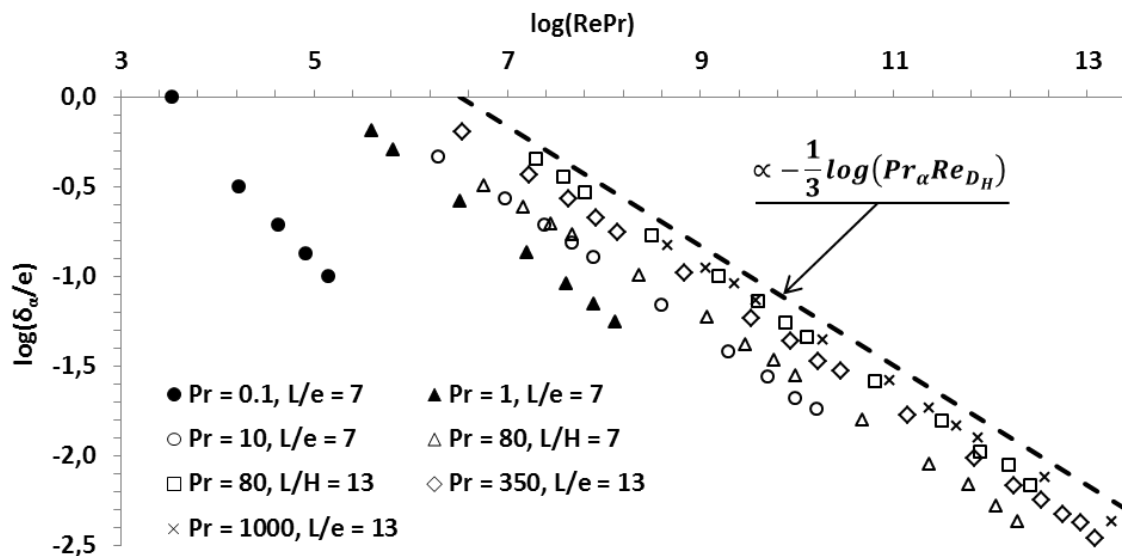
$\overrightarrow{U_{Saff}}$ ↗ ↗

2.4 - SENSIBILITY TO FORCED CONVECTION

o Plume development in a Poiseuille flow :

$$\bullet \frac{\delta_\alpha}{e} \sim \left(\frac{L}{e}\right)^{1/3} Pr_\alpha^{-1/3} Re_{DH}^{-1/3}$$

Relative plume thickness vs. Reynolds-Prandtl (log scale)



**Forced convection
decreases δ_α**

3 – RECENT WORKS & PROSPECTS

Experiments

- High speed camera recorder
- Flow characterization (bubble-induced & forced convection)
- Electrochemical Impedance Spectroscopy

DNS

- Implementation of Lagrangian tracking
- Two-way coupling between the dispersed and continuous phase
- Simulation of collisions between bubbles

ANY QUESTION ?

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