

# CFD Simulation of Pore Pressure Oscillation Method for the Measurement of Permeability in Tight Porous-Media

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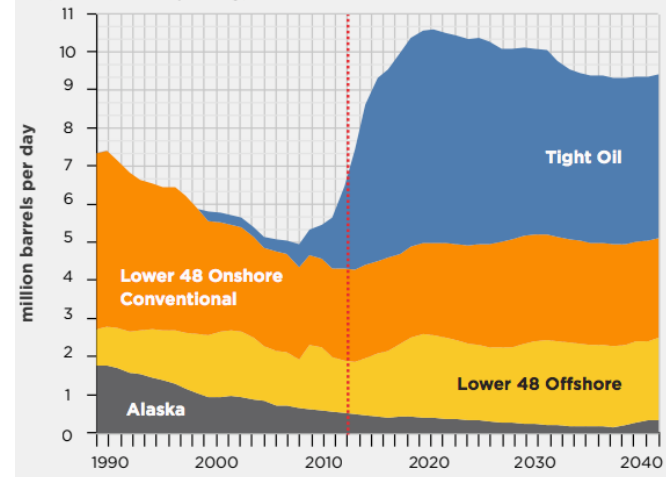
Boston, MA

Oct 5-7, 2016

# Unconventional Hydrocarbon Resources

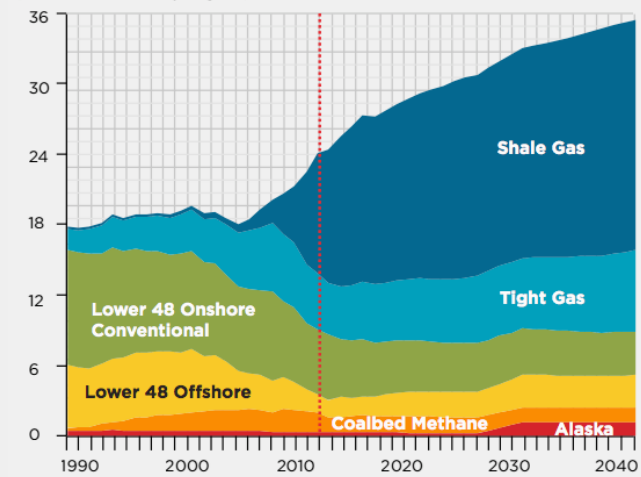
U.S. Crude Oil Production

(million barrels per day)



U.S. Natural Gas Production

(trillion cubic feet per year)

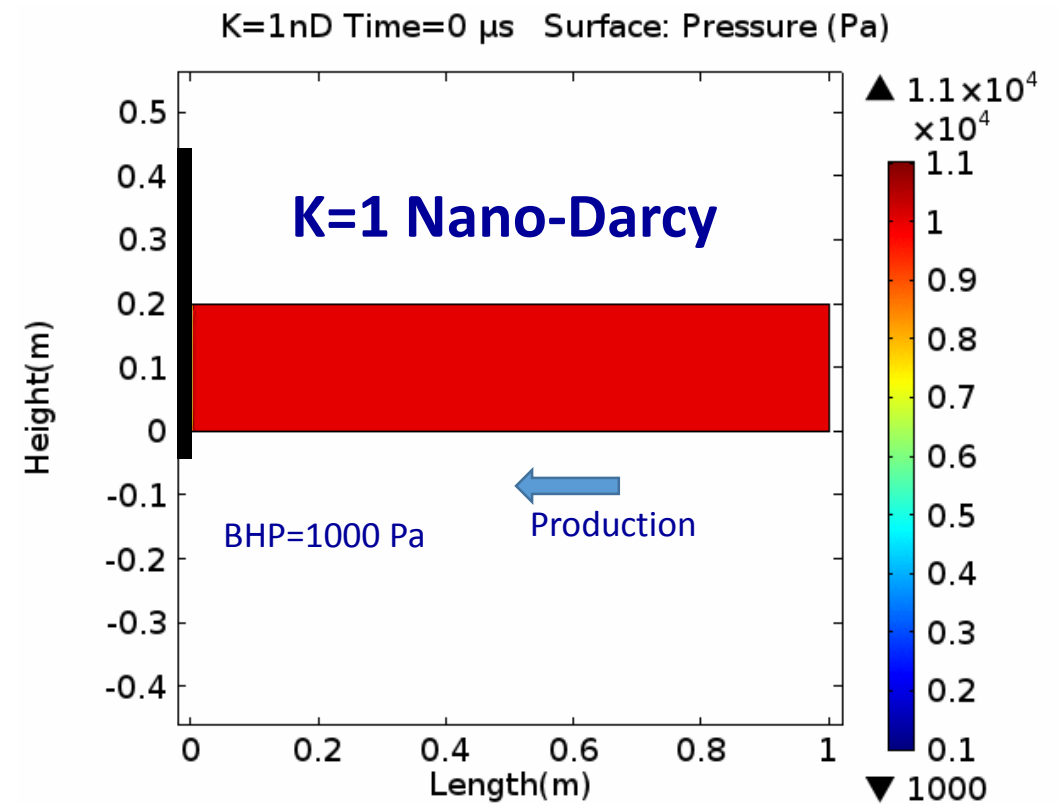
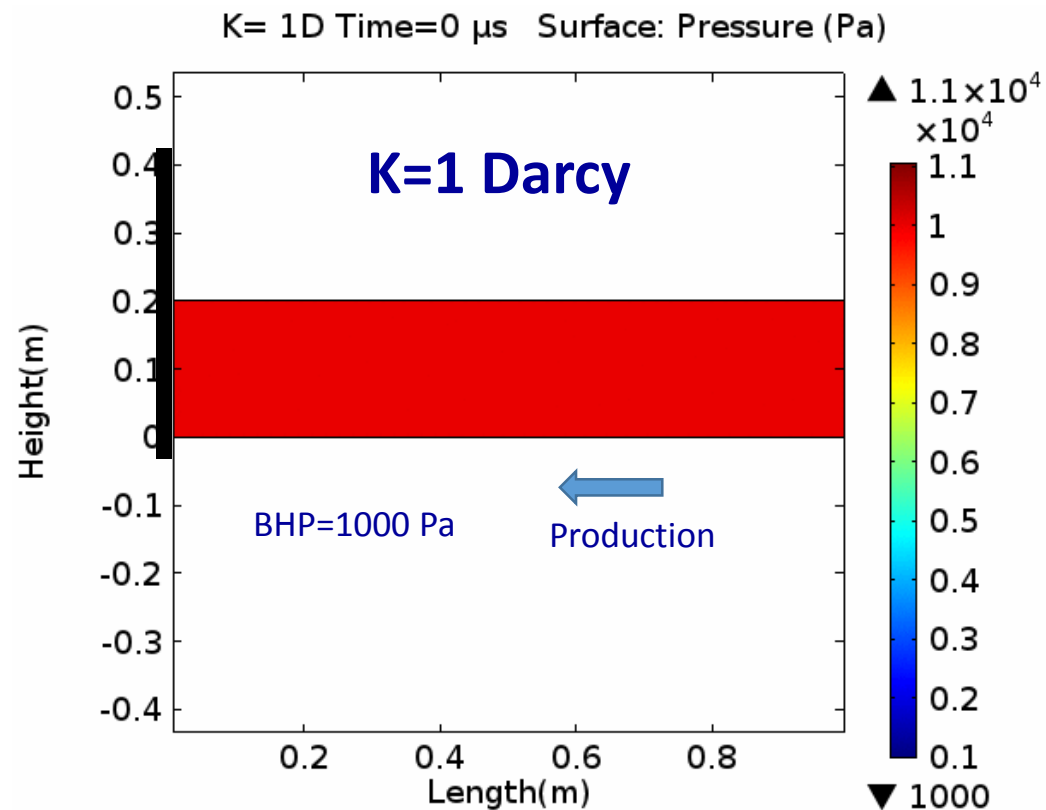


Source: <http://www.api.org>

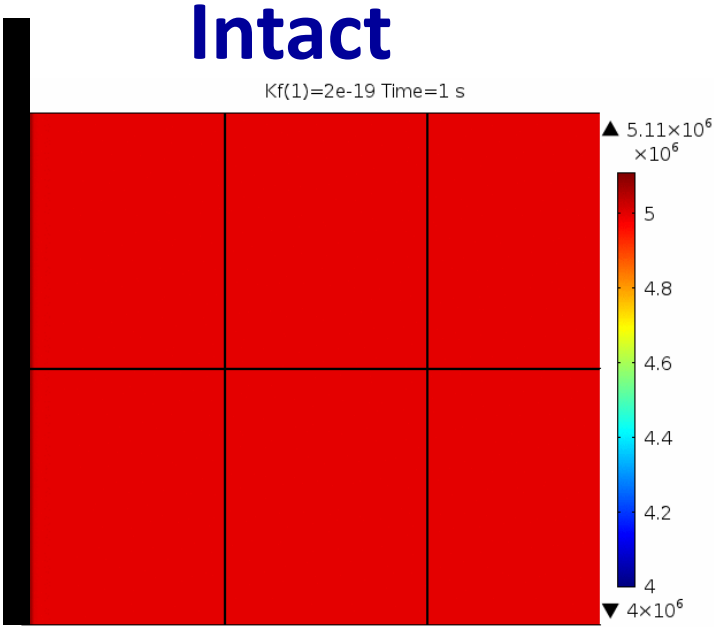


Source: <http://www.ogj.com>

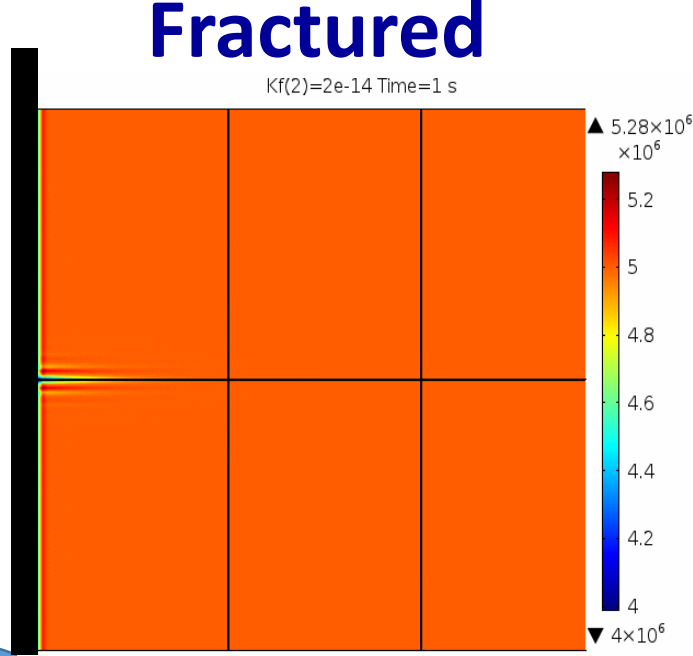
# Conventional vs. Unconventional Reservoirs



# Effect of Fracturing on Production



Sad Pistachio



Smiley Pistachio



Fracturing



# Outline

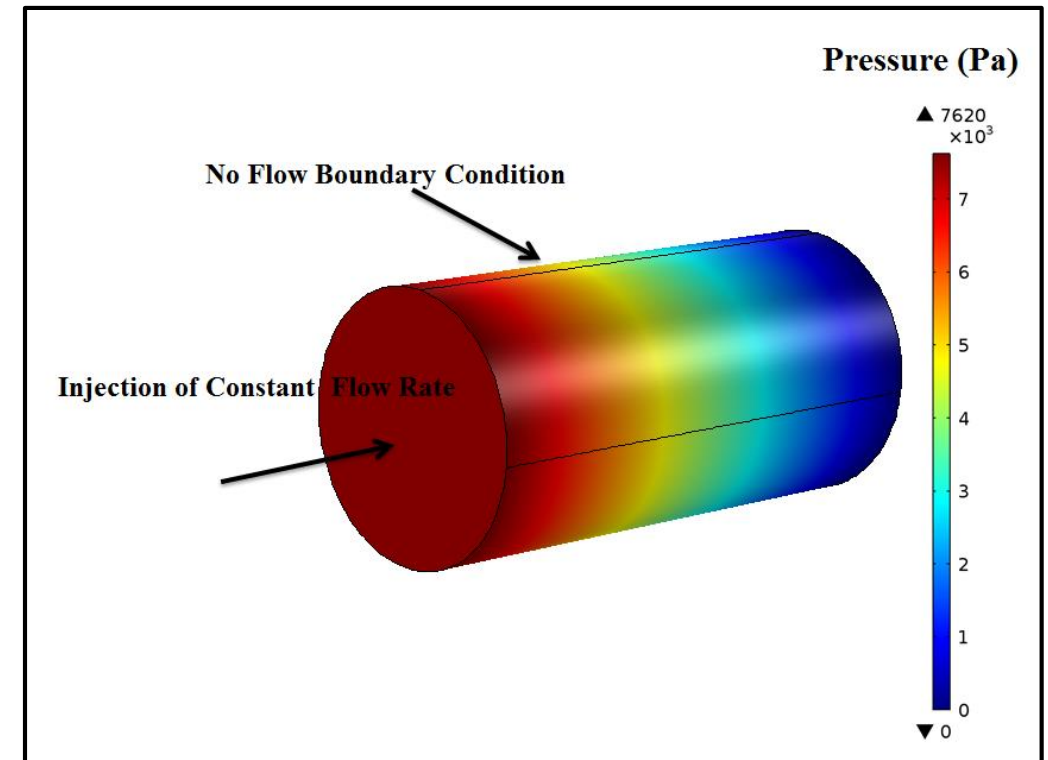
- ✓ Introduction
  - ✓ Steady State Method of Permeability Measurement
  - ✓ Unsteady State Method: Pulse Decay Method
  - ✓ Unsteady State Method: Crushed Sample Method
  
- ✓ Unsteady State Method: Pressure Oscillation Method
  - ✓ How it works?
  - ✓ Theory
  - ✓ Numerical Simulation
  - ✓ Analyze of experimental parameters
  - ✓ Preliminary results on Anisotropy

# Steady State Method of Permeability Measurement

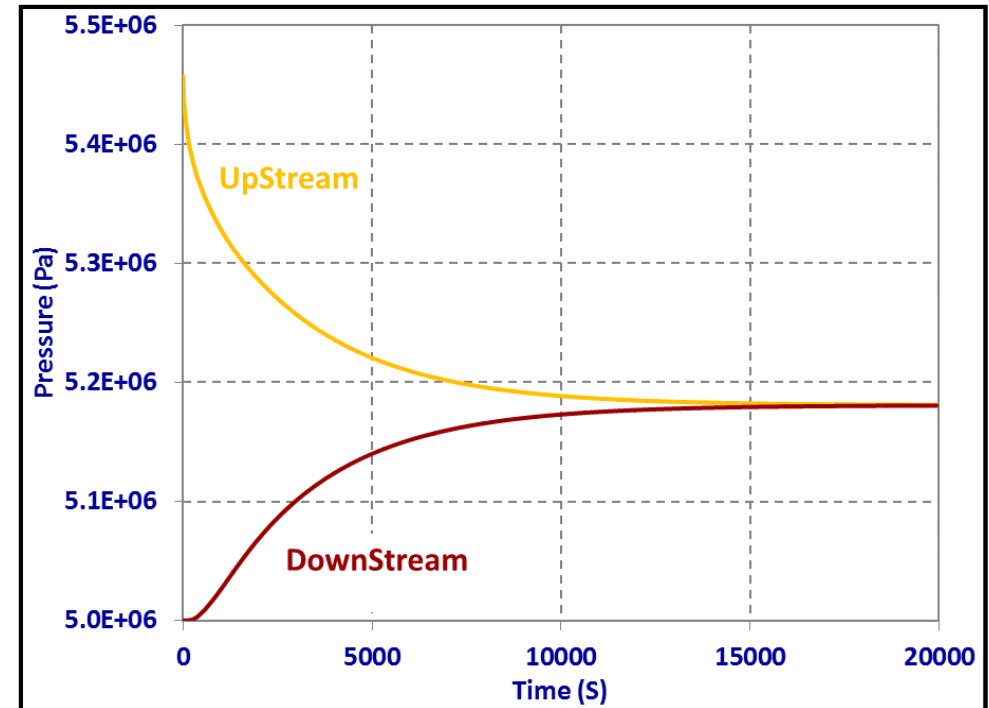
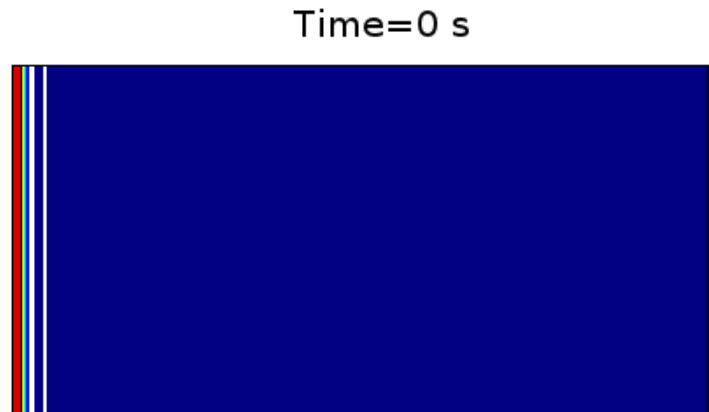
Core analysis and permeability measurement techniques

- Steady state methods
  - ✓ Constant flow or constant pressure head methods
  - ✓ Darcy's equation
  - ✓ Suitable for high permeability samples
  - ✓ Time consuming for low permeability samples (days to weeks)

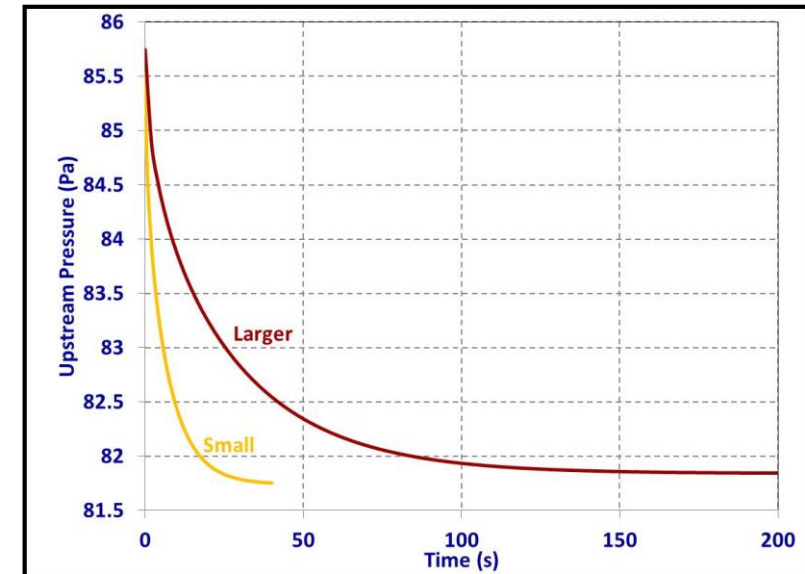
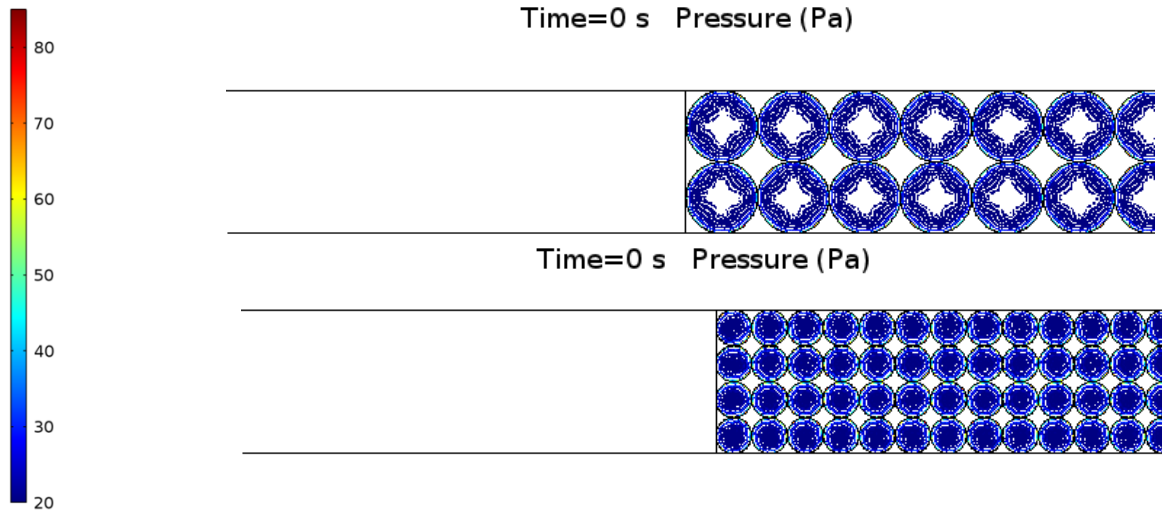
$$\mathbf{k} = \frac{-q\mu L}{A \Delta P}$$



# Unsteady State Method of Permeability Measurement: Pulse Decay Method



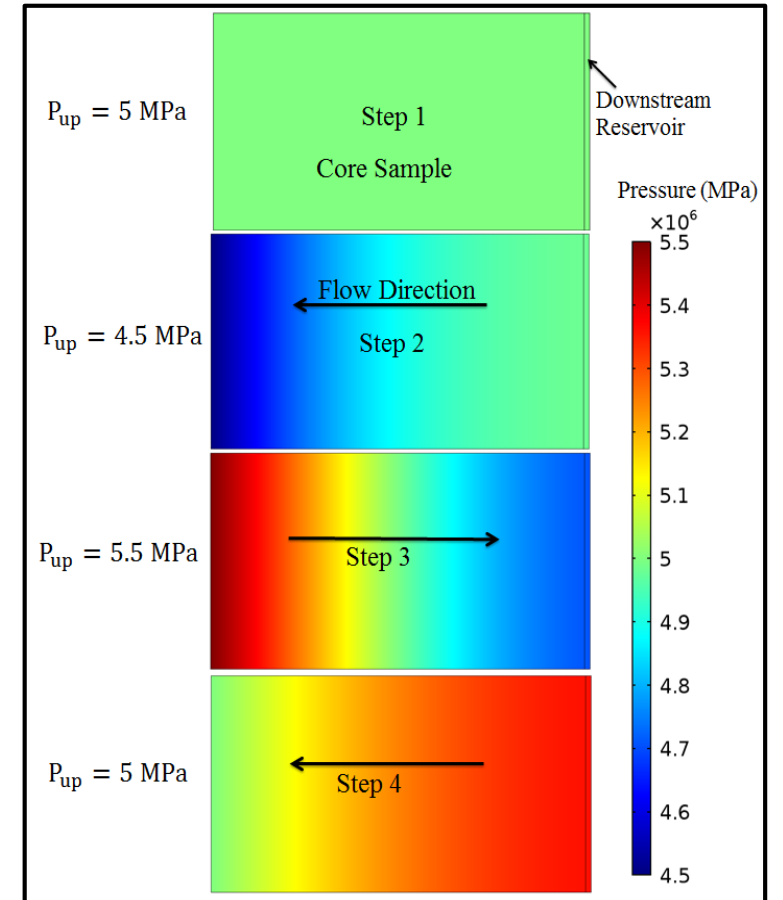
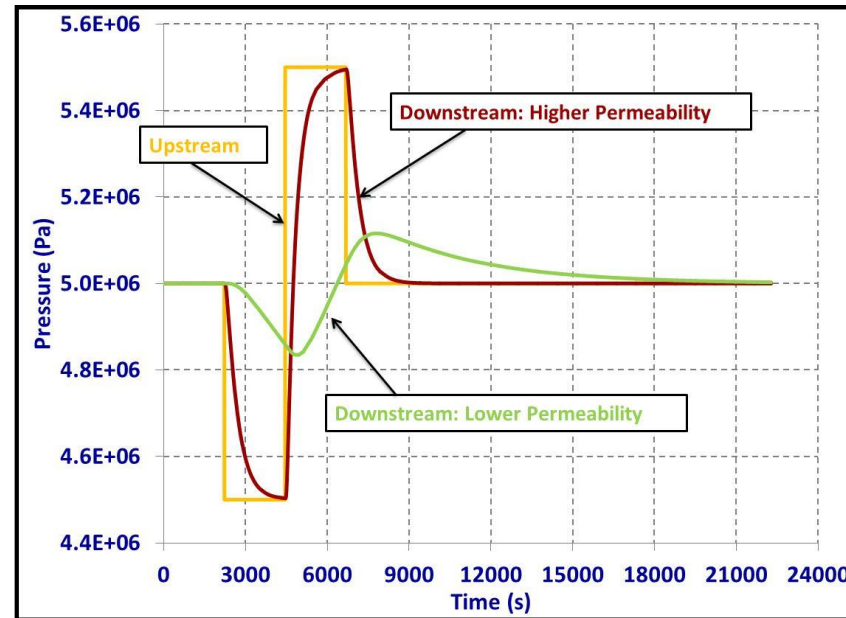
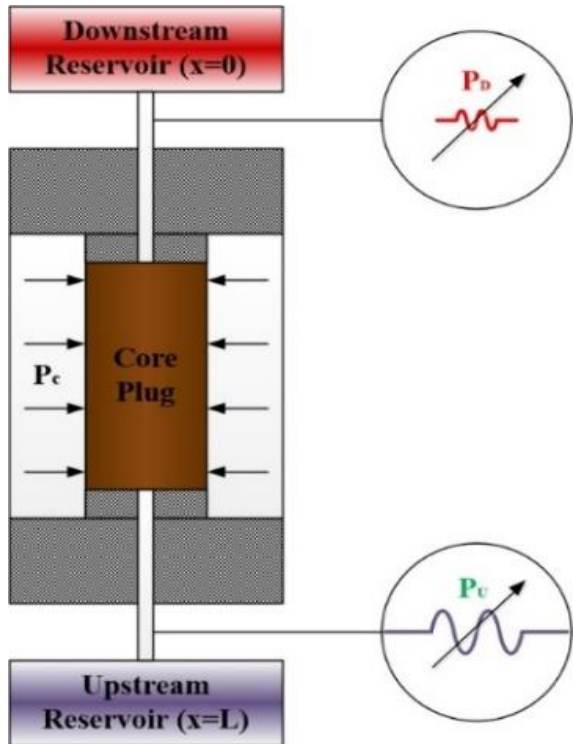
# Unsteady State Method of Permeability Measurement: Crushed Sample Method



**Permeability is Size-Dependent  
in GRI Method**



# Pressure Oscillation Method



Schematic diagram of experimental setup

Pressure data recorded at upstream and downstream reservoirs

## Methodology – (analytical formulation) Kranz et. al. at (1990)

- Governing equations in pressure oscillation method (homogenous and isotropic sample)

$$\begin{array}{l}
 \frac{\partial(\phi\rho)}{\partial t} + \frac{\partial(\rho u)}{\partial x} = 0 \quad \text{Conservation of mass} \\
 u = -\frac{k}{\mu} \frac{dp}{dx} \quad \text{Darcy's equation}
 \end{array}
 \left. \vphantom{\begin{array}{l} \frac{\partial(\phi\rho)}{\partial t} + \frac{\partial(\rho u)}{\partial x} = 0 \\ u = -\frac{k}{\mu} \frac{dp}{dx} \end{array}} \right\} \text{Combined together} \longrightarrow \boxed{\frac{\partial p}{\partial t} - \frac{k}{\mu\beta_s} \frac{\partial^2 p}{\partial x^2} = 0}$$

$\beta_s = \phi / p$

- Governing boundary conditions in pressure oscillation method

$$p(L, t) = P_A \sin(\omega t + \delta), \quad x = L$$

$$\frac{dp}{dt} - \frac{kA}{\mu\beta_d} \frac{\partial p}{\partial x} = 0, \quad x = 0$$

$$\beta_d = V_D / p$$

- Governing initial condition

$$p(x, 0) = p_0$$

## Methodology – (analytical formulation)

- Solution of governing partial differential equation

$$p = \underbrace{\alpha P_A \sin(\omega t + \delta + \vartheta)}_{\text{Permanent solution}} + \underbrace{2P_A \frac{k}{\mu} \beta_s AL \sum_{n=1}^{\infty} \left( \frac{(\beta_s L^2 \omega \cos \delta - \frac{k}{\mu} \psi_n^2 \sin \delta) [\cos(\xi \psi_n) - \frac{\beta_d \psi_n}{\beta_s AL} \sin(\xi \psi_n)]}{((\frac{k}{\mu})^2 \psi_n^4 + \beta_s^2 L^4 \omega^2) [(\beta_d \psi_n^2 + \beta_s AL) \cos \psi_n + (\beta_s AL + 2\beta_d) \sin \psi_n]} \right)}_{\text{Transient and temporary solution}} \psi_n^2 e^{-\frac{k \psi_n^2}{\mu \beta_s L^2} t}$$

Permanent solution

Transient and temporary solution

$$\alpha = \frac{\sqrt{\frac{\beta_s \omega \mu}{2k} (1+i) \cosh\left[\sqrt{\frac{\beta_s \omega \mu}{2k} (1+i)x}\right] + \frac{\beta_d i \omega \mu}{kA} \sinh\left[\sqrt{\frac{\beta_s \omega \mu}{2k} (1+i)x}\right]}{\sqrt{\frac{\beta_s \omega \mu}{2k} (1+i) \cosh\left[\sqrt{\frac{\beta_s \omega \mu}{2k} (1+i)L}\right] + \frac{\beta_d i \omega \mu}{kA} \sinh\left[\sqrt{\frac{\beta_s \omega \mu}{2k} (1+i)L}\right]}}$$

$$\vartheta = \arg \left\{ \frac{\sqrt{\frac{\beta_s \omega \mu}{2k} (1+i) \cosh\left[\sqrt{\frac{\beta_s \omega \mu}{2k} (1+i)x}\right] + \frac{\beta_d i \omega \mu}{kA} \sinh\left[\sqrt{\frac{\beta_s \omega \mu}{2k} (1+i)x}\right]}{\sqrt{\frac{\beta_s \omega \mu}{2k} (1+i) \cosh\left[\sqrt{\frac{\beta_s \omega \mu}{2k} (1+i)L}\right] + \frac{\beta_d i \omega \mu}{kA} \sinh\left[\sqrt{\frac{\beta_s \omega \mu}{2k} (1+i)L}\right]}} \right\}$$

## Methodology – (analytical formulation)

Solution at location of downstream reservoir (x=0)

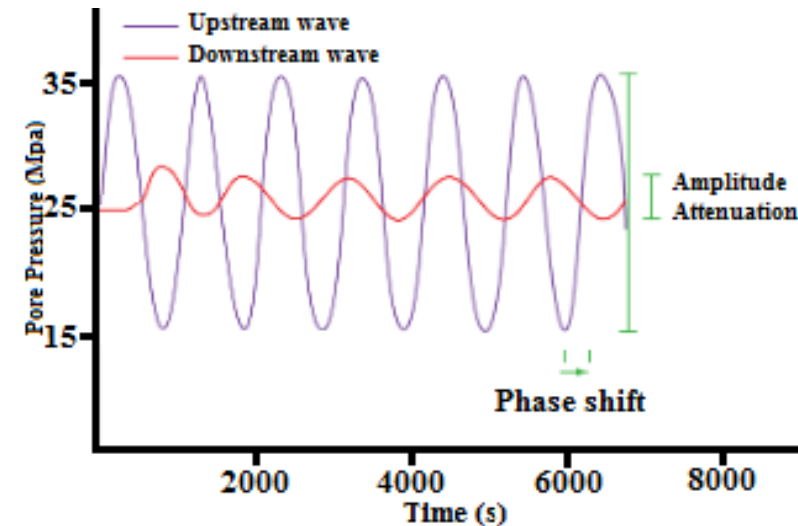
$$A_r e^{-i\theta} = \left( \frac{1+i}{\sqrt{\xi\eta}} \sinh\left[(1+i)\sqrt{\frac{\xi}{\eta}}\right] + \cosh\left[(1+i)\sqrt{\frac{\xi}{\eta}}\right] \right)^{-1}$$

$A_r$  Pressure wave amplitude attenuation from upstream to downstream

$\theta$  Pressure wave phase shift from upstream to downstream

$\xi = \frac{AL\beta_S}{\beta_d}$  Dimensionless porosity

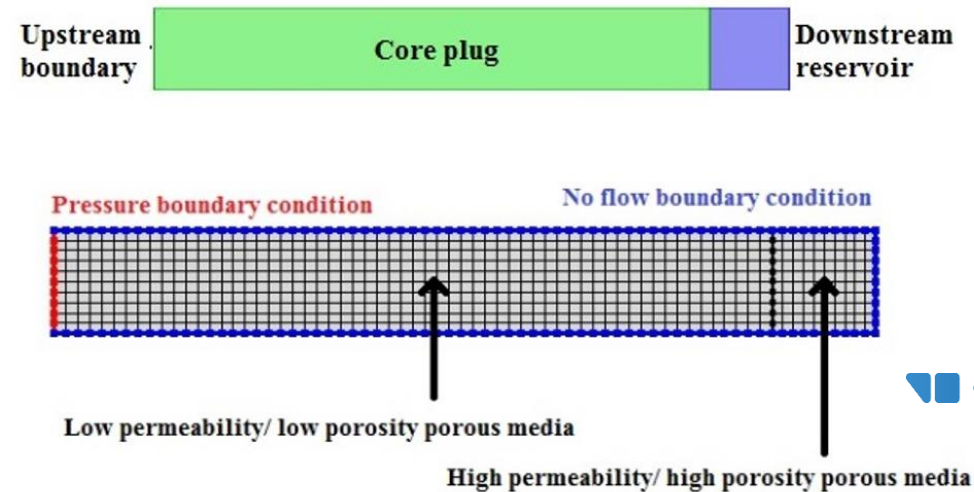
$\eta = \frac{ATk}{\pi L \mu \beta_d}$  Dimensionless permeability



## Methodology – (CFD modeling )

### COMSOL Geometry and computational mesh

- Core length: 50 mm
- Core height: 10 mm
- Downstream reservoir length: variable

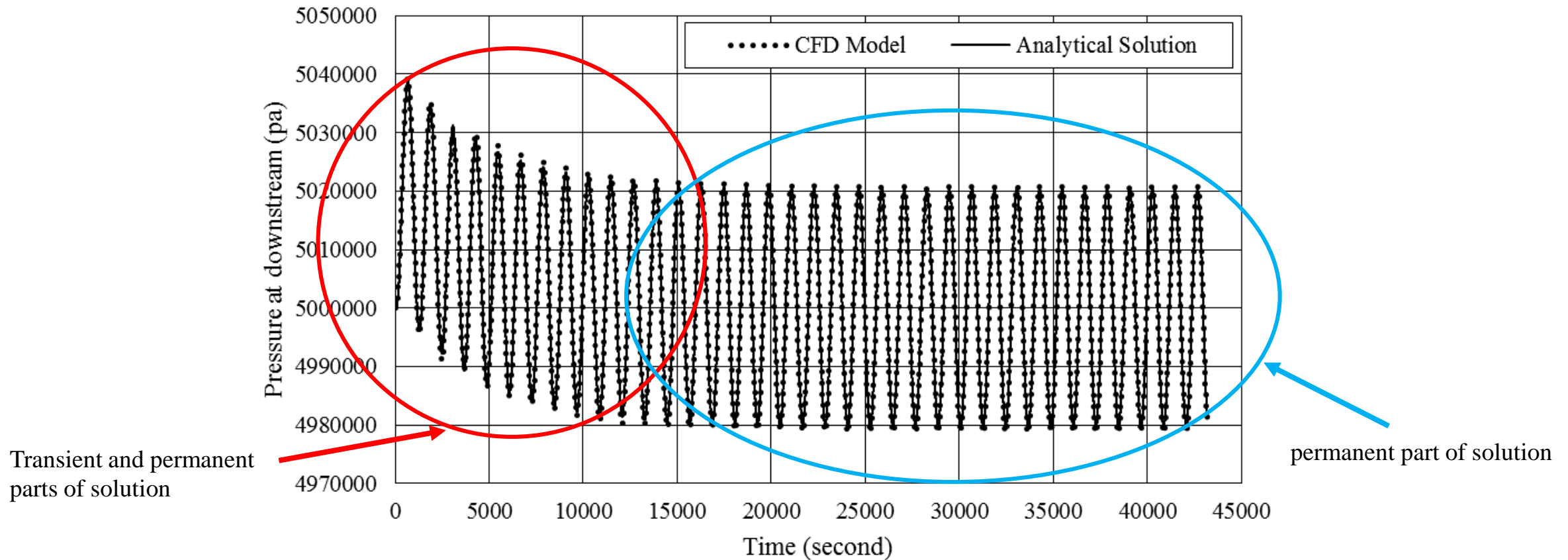


- Mesh size: 1 mm (2D model – quad mesh)
- Aspect ratio: 1
- Time step size: 1 second

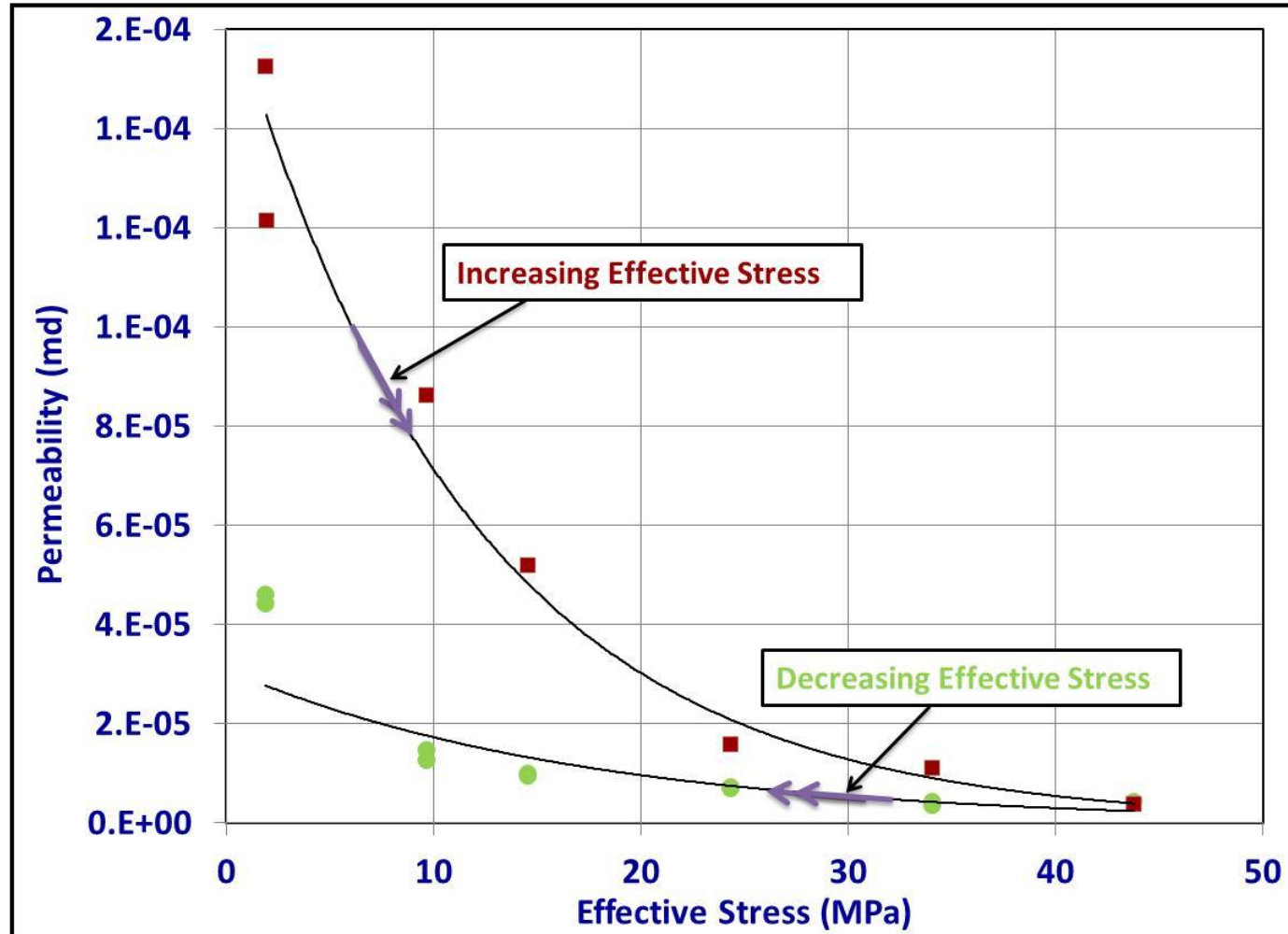
- Time dependent direct solver: Multifrontal Massively Parallel sparse direct Solver (MUMPS)
- Porous media fluid properties: Ideal gas
- Total simulation time: 36 times of pressure wave period (to have only the permanent part of solution)
- Initial pore pressure: 5e6 Pa

## Results and Discussions

Pressure response at downstream reservoir (CFD and analytical solution results)

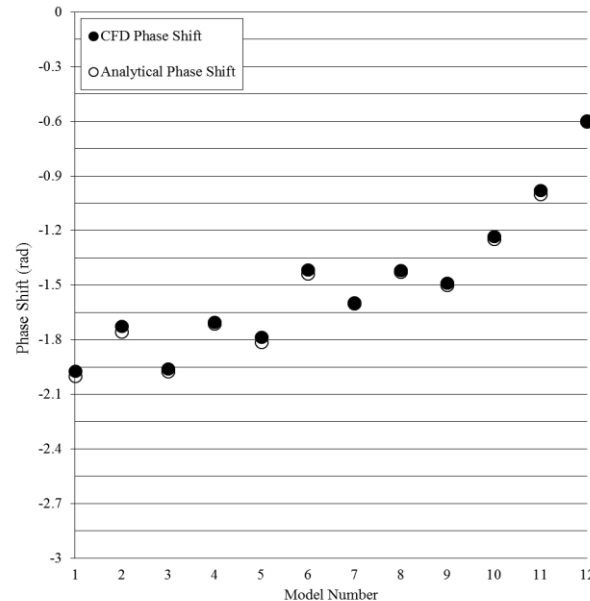
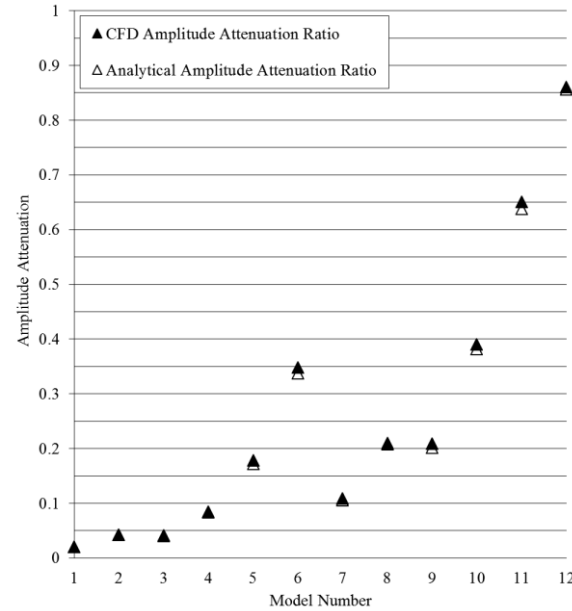


# Analyzing Laboratory Data to Calculate Shale Permeability using Oscillation Method



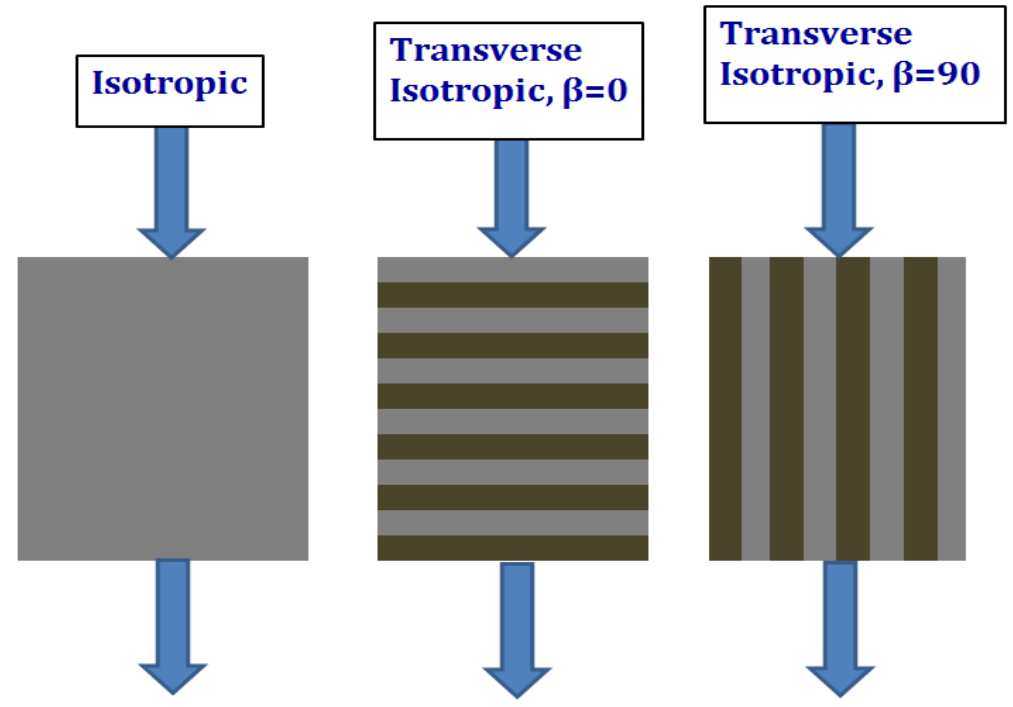
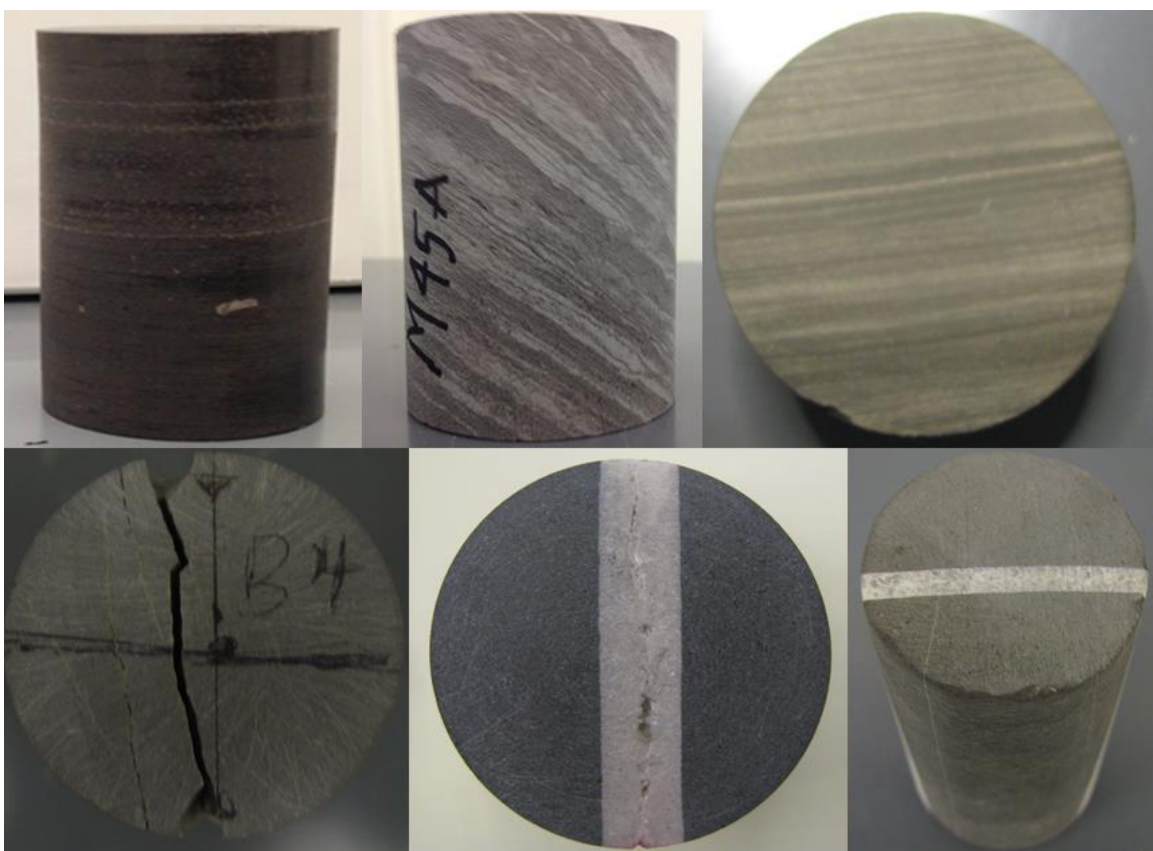
# Methodology – (CFD modeling )

Model	$k(m^2)$	$\varphi$	$L_D (mm)$	$T(s)$
1	$10^{-18}$	0.06	50	1200
2	$10^{-18}$	0.06	50	2400
3	$10^{-18}$	0.06	25	1200
4	$10^{-18}$	0.06	25	2400
5	$10^{-18}$	0.06	5	1200
6	$10^{-18}$	0.06	5	2400
7	$10^{-17}$	0.09	50	600
8	$10^{-17}$	0.09	50	1200
9	$10^{-17}$	0.09	25	600
10	$10^{-17}$	0.09	25	1200
11	$10^{-17}$	0.09	5	600
12	$10^{-17}$	0.09	5	1200



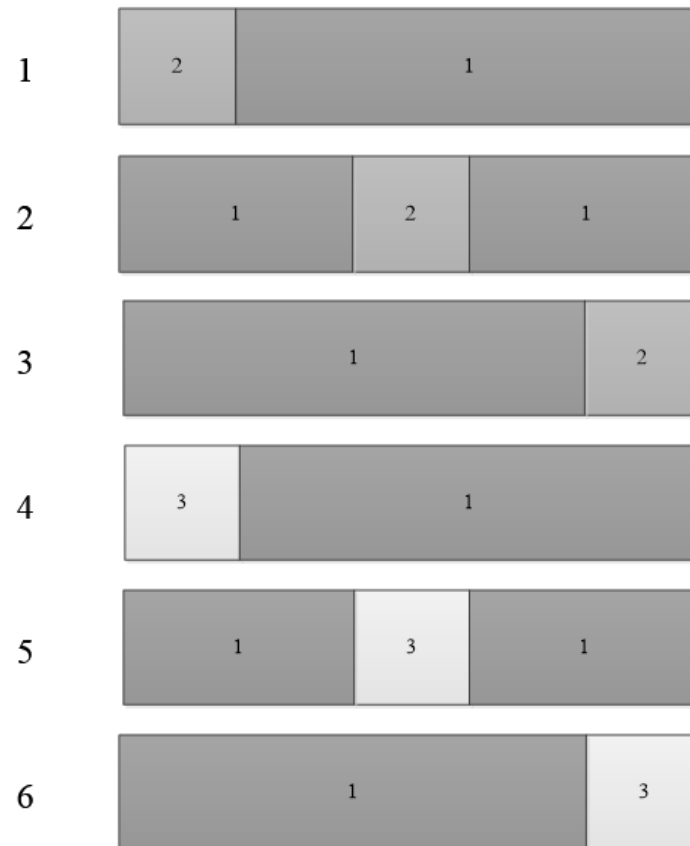


# Anisotropy in Shales



## Results and Discussions

Model number	Amplitude attenuation	Phase shift
1	0.358	-1.376
2	0.345	-1.470
3	0.310	-1.432
4	0.365	-1.357
5	0.352	-1.457
6	0.315	-1.416



- Layer 1
  - Permeability:  $10^{-18} \text{ m}^2$
  - Porosity: 0.06
- Layer 2
  - Permeability:  $10^{-17} \text{ m}^2$
  - Porosity: 0.09
- Layer 3
  - Permeability:  $10^{-16} \text{ m}^2$
  - Porosity: 0.1

## Conclusion

- ✓ Pressure oscillation method was successfully simulated by COMSOL CFD module to calculate the permeability of tight rocks in the range of nano-Darcy.
- ✓ Excellent agreement between CFD and analytical formulation results was observed in isotropic models.
- ✓ Parametric study of simulations is in progress to optimize experiments for permeability measurement.
- ✓ Numerical simulation of anisotropic rocks is in progress to get more accurate interpretation of results in heterogeneous and anisotropic shale formations.

# CFD Simulation of Pore Pressure Oscillation Method for the Measurement of Permeability in Tight Porous-Media

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Thank you!

Any questions?